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ALTITUDE DEVELOPMENTAL TESTING OF THE J-2S ROCKET ENGINE IN PROPULSION ENGINE TEST CELL (J-4) (TESTS J4-1902-01 THROUGH J4-1902-04)

N. R. Vetter ARO, Inc.

February 1969

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LARGE ROCKET FACILITY

ARNOLD ENGINEERING DEVELOPMENT CENTER
AIR FORCE SYSTEMS COMMAND
ARNOLD AIR FORCE STATION, TENNESSEE

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N. R. Vetter ARO, Inc.

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Letter dt d 12 July, 74 Signed William Ol Cole

#### **FOREWORD**

The work reported herein was sponsored by the National Aeronautics and Space Administration (NASA), Marshall Space Flight Center (MSFC) (I-E-J), under System 921E, Project 9194.

The results of the tests presented were obtained by ARO, Inc., (a subsidiary of Sverdrup & Parcel and Associates, Inc.), contract operator of the Arnold Engineering Development Center (AEDC), Air Force Systems Command (AFSC), Arnold Air Force Station, Tennessee, under Contract F40600-69-C-0001. Program direction was provided by NASA/MSFC; technical and engineering liaison was provided by North American Rockwell Corporation, Rocketdyne Division, manufacturer of the J-2S rocket engine, and McDonnell Douglas Corporation, Douglas Aircraft Company, Missile and Space Systems Division, manufacturer of the S-IVB stage. The testing reported herein was conducted between December 5, 1968, and January 10, 1969, in Propulsion Engine Test Cell (J-4) of the Large Rocket Facility (LRF) under ARO Project No. KA1902. The manuscript was submitted for publication on January 24, 1969.

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This technical report has been reviewed and is approved.

Edgar D. Smith
Major, USAF
AF Representative, LRF
Directorate of Test

Roy R. Croy, Jr. Colonel, USAF Director of Test

#### **ABSTRACT**

Five firings of the Rocketdyne J-2S rocket engine (S/N J-111A) were conducted in Test Cell J-4 of the Large Rocket Facility between December 5, 1968, and January 10, 1969. These firings were accomplished during test periods J4-1902-01 through J4-1902-04 at pressure altitudes of approximately 100, 000 ft at engine start to investigate engine idle-mode operation, transition from idle mode to main stage, and steady-state operation at main stage. The engine started successfully in all cases and two planned transitions from idle mode to main stage were accomplished. The thrust chamber and injector were damaged extensively during a 288.5-sec duration idle-mode firing (04A).

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		NOMENCLATURE				
A		Area, in. <sup>2</sup>				
ASI		Augmented spark igniter				
CCP		Customer connect panel				
EBW		Exploding bridge wire				
FM		Frequency modulation				
MFV		Main fuel valve				
MOV		Main oxidizer valve				
O/F		Propellant mixture ratio, oxidizer to fuel, by weight				
SPTS		Solid-propellant turbine starter				
T/C		Thrust chamber				

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t<sub>0</sub> Time at which helium control and idle-mode solenoids are energized; engine start

VSC Vibration safety counts, defined as engine vibration in excess of 150 g rms in a 960- to 6000-Hz frequency range

### SUBSCRIPTS

f Force

m Mass

t Throat

### SECTION I

Testing of the Rocketdyne J-2S rocket engine using an S-IVB battle-ship stage has been in progress since December, 1968, at AEDC. The five firings reported herein were conducted during test periods J4-1902-01 through J4-1902-04 in Propulsion Engine Test Cell (J-4) (Figs. 1 and 2, Appendix I) of the Large Rocket Facility (LRF). These firings were to verify previously obtained test data on the performance of the simplified J-2 engine under simulated altitude conditions. The firings were accomplished at pressure altitudes ranging from 86,000 to 101,000 ft (geometric pressure altitude, Z, Ref. 1) at engine start. Data collected to accomplish the test objectives are presented herein.

### SECTION II

### 2.1 TEST ARTICLE

The test article was a J-2S rocket engine (Fig. 3) designed and developed by Rocketdyne Division of North American Rockwell Corporation. The engine uses liquid oxygen and liquid hydrogen as propellants and is designed to operate either in idle mode at a nominal thrust of 5000 lb<sub>f</sub> and mixture ratio of 2.5 or at main stage at any precalibrated thrust level between 230,000 and 265,000 lb<sub>f</sub> at a mixture ratio of 5.5. The engine design is capable of transition from idle-mode to main-stage operation after a minimum of 1-sec idle mode; from main stage the engine can either be shut down or make a transition back to idle-mode operation before shutdown. An S-IVB battleship stage was used to supply propellants to the engine. A schematic of the battleship stage is presented in Fig. 4.

Listings of major engine components and engine orifices for this test period are presented in Tables I and II, respectively (Appendix II). All engine modifications and component replacements performed during this report period are presented in Tables III and IV, respectively.

### 2.1.1 J-2S Rocket Engine

The J-2S rocket engine (Figs. 3 and 5, Ref. 2) features the following major components:

- 1. Thrust Chamber The tubular-walled, bell-shaped thrust chamber consists of an 18.6-in.-diam combustion chamber with a throat diameter of 12.192 in., a characteristic length (L\*) of 35.4, and a divergent nozzle with an expansion ratio of 40. Thrust chamber length (from the injector flange to the nozzle exit) is 108.6 in. Cooling is accomplished by the circulation of engine fuel flow downward from the fuel manifold through 180 tubes and then upward through 360 tubes to the injector and by film cooling inside the combustion chamber.
- 2. Thrust Chamber Injector The injector is a concentricorificed (concentric fuel orifices around the oxidizer post
  orifices), porous-faced injector. Fuel and oxidizer injector
  orifice areas are 19.2 and 5.9 in.2, respectively. The oxidizer
  portion is compartmentalized, the outer compartment supplying oxidizer during main-stage operation only. The porous
  material, forming the injector face, allows approximately
  3.5 percent of main-stage fuel flow to transpiration cool the
  face of the injector.
- 3. Augmented Spark Igniter The augmented spark igniter unit is mounted on the thrust chamber injector and supplies the initial energy source to ignite propellants in the main combustion chamber. The augmented spark igniter chamber is an integral part of the thrust chamber injector. Fuel and oxidizer are ignited in the combustion area by two spark plugs.
- 4. Fuel Turbopump The fuel turbopump is a one and one-half stage, centrifugal-flow unit, powered by a direct-drive, two-stage turbine. The pump is self lubricated and nominally produces, at the 265,000-lbf-thrust rated condition, a head rise of 60,300 ft of liquid hydrogen at a flow rate of 9750 gpm for a rotor speed of 29,800 rpm.
- 5. Oxidizer Turbopump The oxidizer turbopump is a single-stage, centrifugal-flow unit, powered by a direct-drive, two-stage turbine. The pump is self lubricated and nominally produces, at the 265,000-lbf-thrust rated condition, a head rise of 3250 ft of liquid oxygen at a flow rate of 3310 gpm for a rotor speed of 10,500 rpm.
- 6. Propellant Utilization Valve The motor-driven propellant utilization valve is mounted on the oxidizer turbopump and bypasses liquid oxygen from the discharge to the inlet side of the pump to vary engine mixture ratio.
- 7. Main Oxidizer Valve The main oxidizer valve is a pneumatically actuated, two-stage, butterfly-type valve located in the

oxidizer high pressure duct between the turbopump and the injector. The first-stage actuator positions the main oxidizer valve at the 10-deg position to obtain initial main-stage-phase operation; the second-stage actuator ramps the main oxidizer valve full open to accelerate the engine to the main-stage operating level.

- 8. Main Fuel Valve The main fuel valve is a pneumatically actuated butterfly-type valve located in the fuel high pressure duct between the turbopump and the fuel manifold.
- 9. Pneumatic Control Package The pneumatic control package controls all pneumatically operated engine valves and purges.
- 10. Electrical Control Assembly The electrical control assembly provides the electrical logic required for proper sequencing of engine components during operation. The logic requires a minimum of 1-sec idle-mode operation before transition to main stage.
- 11. Flight Instrumentation Package The instrumentation package contains sensors required to monitor critical engine parameters. The package provides environmental control for the sensors.
- 12. Helium Tank The helium tank has a volume of 4000 in.<sup>3</sup> and provides a helium pressure supply to the engine pneumatic control system for three complete engine operational cycles.
- 13. Thrust Chamber Bypass Valve The thrust chamber bypass valve is a pneumatically operated, normally open, butterfly-type valve which allows fuel to bypass the thrust chamber body during idle-mode operation.
- 14. Idle-Mode Valve The idle-mode valve is a pneumatically operated ball-type valve which supplies liquid oxygen to the idle-mode compartment of the thrust chamber injector during both idle-mode and main-stage operation.
- 15. Hot Gas Tapoff Valve The hot gas tapoff valve is a pneumatically operated butterfly-type valve which provides on-off control of combustion chamber gases to drive the propellant turbopumps.
- 16. Solid-Propellant Turbine Starter The solid-propellant turbine starter provides the initial driving energy (transition to main stage) for the propellant turbopumps to prime the propellant feed systems and accelerate the turbopumps to 75 percent of their main-stage operating level. A three-start capability is provided.

### 2.1.2 S-IVB Battleship Stage

The S-IVB battleship stage, which is mechanically configured to simulate the S-IVB flightweight vehicle, is approximately 22 ft in diameter and 49 ft long and has a maximum propellant capacity of 46,000 lb of liquid hydrogen and 199,000 lb of liquid oxygen. The propellant tanks, fuel above oxidizer, are separated by a common bulkhead. Propellant prevalves, in the low pressure ducts (external to the tanks) interfacing the stage and engine, retain propellants in the stage until being admitted into the engine to the main propellant valves and serve as emergency engine shutoff valves. Vent and relief valve systems are provided for both propellant tanks.

Pressurization of the fuel and oxidizer tanks was accomplished by facility systems using hydrogen and helium, respectively, as the pressurizing gases. The engine-supplied gaseous hydrogen and gaseous oxygen for fuel and oxidizer tank pressurization during flight were routed to the respective facility venting systems.

#### 2.2 TEST CELL

Propulsion Engine Test Cell J-4, Fig. 2, is a vertically oriented test unit designed for static testing of liquid-propellant rocket engines and propulsion systems at pressure altitudes of 100,000 ft. The basic cell construction provides a 1.5-million-lbf-thrust capacity. The cell consists of four major components (1) test capsule, 48 ft in diameter and 82 ft in height, situated at grade level and containing the test article; (2) spray chamber, 100 ft in diameter and 250 ft in depth, located directly beneath the test capsule to provide exhaust gas cooling and dehumidification; (3) coolant water, steam, nitrogen (gaseous and liquid). hydrogen (gaseous and liquid), and liquid oxygen and gaseous helium storage and delivery systems for operation of the cell and test article; and (4) control building, containing test article controls, test cell controls, and data acquisition equipment. Exhaust machinery is connected with the spray chamber and maintains a minimum test cell pressure before and after the engine firing and exhausts the products of combustion from the engine firing. Before a firing, the facility steam ejector, in series with the exhaust machinery, provides a pressure altitude of 100,000 ft in the test capsule. A detailed description of the test cell is presented in Ref. 3.

The battleship stage and the J-2S engine were oriented vertically downward on the centerline of the diffuser-steam ejector assembly. This assembly consisted of a diffuser duct (20 ft in diameter by 150 ft

in length), a centerbody steam ejector within the diffuser duct, a diffuser insert (13.5 ft in diameter by 30 ft in length) at the inlet to the diffuser duct, and a gaseous nitrogen annular ejector above the diffuser insert. The diffuser insert was provided for dynamic pressure recovery of the engine exhaust gases and to maintain engine ambient pressure altitude (attained by the steam ejector) during the engine firing. The annular ejector was provided to suppress steam recirculation into the test capsule during steam ejector shutdown. The test cell was also equipped with (1) a gaseous nitrogen purge system for continuously inerting the normal air in-leakage of the cell; (2) a gaseous nitrogen repressurization system for raising test cell pressure, after engine cutoff, to a level equal to spray chamber pressure and for rapid emergency inerting of the capsule; and (3) a spray chamber liquid nitrogen supply and distribution manifold for initially inerting the spray chamber and exhaust ducting and for increasing the molecular weight of the hydrogen-rich exhaust products.

Systems were provided for temperature conditioning of engine components. Cold helium from a liquid hydrogen-helium heat exchanger was routed externally over the main fuel valve to provide the required temperature. Temperature-conditioned nitrogen from liquid nitrogen-steam vaporizers was routed through shrouds surrounding the solid-propellant turbine starters to provide the required temperatures.

#### 2.3 INSTRUMENTATION

Instrumentation systems were provided to measure engine, stage, and facility parameters. The engine instrumentation was comprised of (1) flight instrumentation for the measurement of critical engine parameters and (2) facility instrumentation which was provided to verify the flight instrumentation and to measure additional engine parameters. The flight instrumentation was provided and calibrated by the engine manufacturer; facility instrumentation was initially calibrated and periodically recalibrated at AEDC. Appendix III contains a list of all measured engine test parameters and the locations of selected sensing points.

Pressure measurements were made using strain-gage and capacitance-type pressure transducers. Temperature measurements were made using resistance temperature transducers and thermocouples. Oxidizer and fuel turbopump shaft speeds were sensed by magnetic pick-up. Fuel and oxidizer flow rates to the engine were measured by turbine-type flowmeters which are an integral part of the engine. Vibrations were measured by accelerometers mounted on the oxidizer injector

dome and on the turbopumps. Primary engine and stage valves were instrumented with linear potentiometers and limit switches.

The data acquisition systems were calibrated by (1) precision electrical shunt resistance substitution for the pressure transducers and resistance temperature transducer units; (2) voltage substitution for the thermocouples; (3) frequency substitution for shaft speeds and flowmeters; and (4) frequency-voltage substitution for accelerometers and the capacitance-type pressure transducer.

The types of data acquisition and recording systems used during this test period were (1) a multiple-input digital data acquisition system scanning each parameter at 40 samples per second (50 samples per second for firing 04A) and recording on magnetic tape; (2) single-input, continuous-recording FM systems recording on magnetic tape; (3) photographically recording galvanometer oscillographs; (4) direct-inking, null-balance, potentiometer-type X-Y plotters and strip charts; and (5) optical data recorders. Applicable systems were calibrated before each test (atmospheric and altitude calibrations). Television cameras, in conjunction with video tape recorders, were used to provide visual coverage during an engine firing, as well as for replay capability for immediate examination of unexpected events.

### 2.4 CONTROLS

Control of the J-2S engine, battleship stage, and test cell systems during the terminal countdown was provided from the test cell control room. A facility control logic network was provided to interconnect the engine control system, major stage systems, the engine safety cutoff system, the observer cutoff circuits, and the countdown sequencer. A schematic of the engine start control logic is presented in Fig. 6. The sequence of engine events for start and shutdown is presented in Figs. 7a and b.

# SECTION III PROCEDURE

Preoperational procedures were begun several hours before the test period. All consumable storage systems were replenished, and engine inspections, leak checks, and drying procedures were conducted. Propellant tank pressurants and engine pneumatic and purge gas samples were taken to ensure that specification requirements were met. Chemical analysis of propellants was provided by the propellant suppliers.

Facility sequence, engine sequence, and engine abort checks were conducted within a 24-hr time period before an engine firing to verify the proper sequence of events. Facility and engine sequence checks consisted of verifying the timing of valves and events to be within specified limits; the abort checks consisted of electrically simulating engine malfunctions to verify the occurrence of an automatic engine cutoff signal. A final engine sequence check was conducted immediately preceding the test period.

Oxidizer dome and thrust chamber jacket purges were initiated before evacuating the test cell. After completion of instrumentation calibrations at atmospheric conditions, the solid-propellant turbine starters were installed, the test cell was evacuated to approximately 0.5 psia with the exhaust machinery, and instrumentation calibrations at altitude conditions were conducted. Immediately before loading propellants on board the vehicle, the cell and exhaust-ducting atmosphere was inerted. At this same time, the cell nitrogen purge was initiated for the duration of the test period, except for engine mainstage operation. The vehicle propellant tanks were then loaded, and the remainder of the terminal countdown was conducted. Temperature conditioning of the various engine components was accomplished as required, using the facility-supplied engine component conditioning system. Table V presents the engine purges and thermal conditioning operations during the terminal countdown and immediately following the engine firing.

# SECTION IV RESULTS AND DISCUSSION

### 4.1 TEST SUMMARY

Five firings of the Rocketdyne J-2S rocket engine (S/N J-111A) were conducted between December 5, 1968, and January 10, 1969, during test periods J4-1902-01 through J4-1902-04. These firings comprised the initial testing of the J-2S engine at altitude conditions; pressure altitude at engine start ranged from 86,000 to 101,000 ft.

Test requirements and specific test results are summarized in Table VI. Start and shutdown transient operating times for selected engine valves are presented in Table VII. Figure 8 shows engine start conditions for propellant pump inlets and helium tank. Accumulated firing durations were 593.8 sec in idle mode and 39.1 sec of mainstage operation.

Data presented in subsequent sections are from the digital data acquisition system except where indicated otherwise. Propellant flow rates are based on engine flowmeter calibration constants supplied by the engine manufacturer: 5.50 and 2.00 cycles/gal for the oxidizer and fuel flowmeters, respectively.

### 4.2 TEST RESULTS

### 4.2.1 Firing J4-1902-01A

Firing 01A was a 172.3-sec duration idle-mode firing to evaluate (1) thrust chamber chilldown rate, (2) augmented spark igniter performance, (3) engine mixture ratio, (4) helium consumption rate, and (5) engine integrity. Engine ambient and combustion chamber pressures are shown in Fig. 9; pressure altitude at engine start was 99,000 ft. At  $t_0 + 42$  sec a facility malfunction resulted in an engine ambient pressure and temperature level which adversely affected engine performance. Data beyond  $t_0 + 42$  sec which are not considered representative of J-2S engine operation at altitude conditions are not presented.

Thrust chamber chilldown rate as indicated by external skin thermocouples at the engine throat and exit is shown in Fig. 10. Augmented spark igniter performance is shown in Fig. 11; ignition was detected at  $t_0 + 0.364$  sec. Engine propellant flow rate and mixture ratio data in Fig. 12 were based on pump discharge temperatures and pressures and a manual reduction of the flowmeter cyclic outputs as recorded on an oscillogram. Included in Fig. 12 are engine inlet and combustion chamber pressures. Helium consumption and engine integrity data are presented in Sections 4.2.7 and 4.2.8, respectively.

### 4.2.2 Firing J4-1902-02A

This was a 32.2-sec duration main-stage firing to evaluate (1) engine start and shutdown transients, (2) steady-state operation, (3) solid-propellant turbine starter performance, (4) oxidizer system pressure surges, and (5) engine-generated side loads. Pressure altitude at engine start was 99,000 ft; engine ambient and combustion chamber pressures are shown in Fig. 13. The ambient pressure increase beginning at t<sub>0</sub> + 7 sec was caused by inadvertant operation of the facility annular ejector.

Engine start and shutdown transients and steady-state operation were satisfactory, as shown in Fig. 14. At  $t_0$  + 7 sec a propellant utilization valve excursion was made to produce a mixture ratio of 5.44

and a peak combustion chamber pressure of 1215 psia at t<sub>0</sub> + 27 sec. Solid-propellant turbine starter performance is shown in Fig. 15. Combustion pressure measurement was not recovered, but satisfactory starter performance is shown by the propellant pump start transients (Fig. 14). A maximum oxidizer system pressure of 1460 psia (230 psi above the operating level) was measured at the oxidizer pump discharge at t<sub>0</sub> + 33.45 sec as shown in Fig. 16. Engine-generated side loads were less than 1200 lbf, as shown in Fig. 17. The indicated levels before engine start result from tare loads caused by engine propellant supply line pressures and temperatures; the indicated oscillations before engine start result from the operation of facility steam and cooling water systems. Fuel pump start transient performance is shown in Fig. 18.

### 4.2.3 Firing J4-1902-03A

This firing consisted of 76.2 sec of idle-mode operation followed by a transition to main stage. Primary objectives were to evaluate (1) thrust chamber chilldown, (2) augmented spark igniter performance, (3) idle-mode mixture ratio, (4) engine transition from idle-mode to main-stage operation, (5) solid-propellant turbine starter performance, and (6) oxidizer system pressure surges. Pressure altitude at engine start was 86,000 ft; engine ambient and combustion chamber pressures are shown in Fig. 19.

Thrust chamber chilldown data are indicated in Fig. 20. The thrust chamber chilldown rate compares closely with that indicated for firing 01A. Augmented spark igniter performance is shown in Fig. 21; ignition was detected at  $t_0 + 0.481$  sec compared to 0.364 sec for firing 01A. Engine propellant flow rate and mixture ratio data in Fig. 22 were calculated in the same manner as those presented for firing 01A. Engine inlet and combustion chamber pressures are included in Fig. 22.

Transition from idle-mode to main-stage operation is shown in Fig. 23. Transition was satisfactory and compares favorably with firing 02A. Solid-propellant turbine starter performance (Fig. 24) was consistent with that obtained during firing 02A. Combustion pressure (Fig. 24a) was as predicted by the engine manufacturer. The burn duration was 2.4 sec, and the maximum pressure was 3420 psia. A maximum oxidizer system pressure (Fig. 25) of 1340 psia was measured at the oxidizer pump discharge at  $t_0 + 83.38$  sec. This was 120 psi less than that measured during firing 02A.

Fuel pump start transient performance is shown in Fig. 26. Data analysis indicated a possible degradation in the fuel pump balance piston rings, and the engine manufacturer requested that no further main-stage testing be conducted until the pump could be repaired or replaced.

### 4.2.4 Firing J4-1902-03B

Firing 03B was a 55.8-sec duration idle-mode firing to evaluate (1) thrust chamber childown, (2) augmented spark igniter performance, and (3) engine mixture ratio. Engine ambient and combustion chamber pressures are shown in Fig. 27; pressure altitude at engine start was 101,000 ft.

Thrust chamber chilldown rate (Fig. 28) compared favorably with that obtained for firings 01A and 03A. Augmented spark igniter performance was satisfactory, as shown in Fig. 29; ignition was detected at  $t_0 + 0.371$  sec. Engine propellant flow rate and mixture ratio data shown in Fig. 30 were calculated as stated in Section 4.2.1. Engine inlet and combustion chamber pressures are included in Fig. 30.

### 4.2.5 Firing J4-1902-04A

Firing 04A was a 288.5-sec duration idle-mode firing to evaluate (1) thrust chamber childown rate, (2) augmented spark igniter performance, and (3) engine mixture ratio. Pressure altitude at engine start was 98,000 ft; engine ambient and combustion chamber pressures are shown in Fig. 31.

Thrust chamber chilldown rate, as shown in Fig. 32, was lower than that measured for firings 01A, 03A, and 03B. The time required to reach a stable temperature was approximately 35 sec, some 10 sec longer than required for firings 01A, 03A, and 03B. Augmented spark igniter performance is shown in Fig. 33; ignition was detected at  $t_0 + 0.412$  sec. Engine propellant flow rate and mixture ratio data shown in Fig. 34 were calculated as stated in Section 4.2.1. Engine inlet and combustion chamber pressures are included in Fig. 34.

Post-test inspection showed that the engine had been damaged extensively during this firing. The injector face had been burned through in two separate places (Fig. 35a), and the ends of several oxidizer posts had been burned and distorted. The combustion chamber tubes (upstream of the throat) in approximately 28 isolated areas had been ruptured and distorted with no evidence of heat damage (Fig. 35b).

Data analysis showed severe pressure perturbations in the combustion chamber and propellant systems beginning at  $t_0 + 158$  sec and recurring at random time intervals until approximately  $t_0 + 252$  sec, at which time combustion chamber pressure decreased to 4.5 psia and remained stable until engine shutdown at  $t_0 + 288.5$  sec. The data shown in Fig. 36 are typical of the pressure perturbations as recorded by the digital data acquisition system. A pressure increase of 412 psi was reduced from the oscillogram recording of oxidizer injector pressure POJ-2 at  $t_0 + 158.20$  sec. No failure analysis is attempted in this report.

### 4.2.6 Idle-Mode Mixture Ratio

Figure 37 shows idle-mode mixture ratio predicted by the engine manufacturer as a function of propellant pump inlet pressures. The predicted mixture ratio assumes saturated liquids at the pump inlets. The measured mixture ratio data are from manual reductions of flowmeter cyclic outputs over 0.5-sec increments as recorded on an oscillogram. The symbols (Fig. 37) are predicted mixture ratio as a function of measured pump inlet pressures. The numbers in parentheses are measured mixture ratio. A portion of the erratic nature of the data in Fig. 37 is attributed to the fact that propellant quality at the oxidizer flowmeter is not known in all cases. The times shown (Fig. 37) were chosen to represent data for which the oxidizer pump discharge pressures and temperatures indicated 100-percent liquid, except firing 03A, for which liquid was not indicated until after shutdown. For firing 04A, liquid was not indicated before to + 140 sec. In all cases shown, the fuel pump discharge pressures and temperatures indicated 100-percent liquid.

### 4.2.7 Helium Consumption

Figure 38 shows temperature and pressure in the engine-mounted helium tank as functions of time for the five firings in this testing period. Helium consumption rate as indicated by a mass change averaged 0.001  $\rm lb_m/sec$  for idle-mode operation and 0.002  $\rm lb_m/sec$  for main-stage operation.

### 4.2.8 Engine Integrity

The main oxidizer valve was replaced following firing 01A because of a leaking idler arm shaft seal. The oxidizer dome purge check valve was repaired because of reverse flow following firing 01A and was replaced following firing 03B. The oxidizer idle-mode line purge check valve was replaced following firing 01A because of reverse flow.

Following firing 02A, the seal between the main oxidizer valve and the high pressure oxidizer supply duct was replaced because of leakage. At this time the oxidizer dome purge check valve was repaired to eliminate reverse flow.

Analysis of data from firing 03A indicated that the fuel pump balance piston rings had degraded to a degree that required repair or pump replacement before any further main-stage operation.

Inspection following firing 04A showed that the engine thrust chamber and injector had been damaged extensively and would require replacement.

# SECTION V SUMMARY OF RESULTS

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Results of testing the J-2S rocket engine in Test Cell J-4 during test periods J4-1902-01 through J4-1902-04 between December 5, 1968, and January 10, 1969, are summarized as follows:

- 1. Augmented spark igniter performance was satisfactory, and engine start was successful in all cases.
- 2. Transition from idle-mode to main-stage operation was successful in all cases.
- 3. Engine-generated side loads during transition to main-stage operation were less than 1200 lb<sub>f</sub>.
- 4. Possible degradation of the fuel pump balance piston rings occurred during main-stage firing 03A.
- 5. The engine thrust chamber and injector were damaged extensively during a 288.5-sec duration idle-mode firing (04A).
- 6. Thrust chamber temperatures reached a steady-state idlemode operating level within 40 sec after engine start.

### REFERENCES

- 1. Dubin, M., Sissenwine, N., and Wexler, H. <u>U.S. Standard</u> Atmosphere, 1962. December 1962.
- 2. "J-2S Interface Criteria." Rocketdyne Document J-7211, October 16, 1967.
- 3. Test Facilities Handbook (7th Edition). "Large Rocket Facility,
  Vol. 3." Arnold Engineering Development Center, July 1968.
- 4. "Engine Model Specification Oxygen/Hydrogen Liquid-Propellant Rocket Engine Rocketdyne Model J-2S." Rocketdyne Document R-2158dS, August 21, 1968.

### APPENDIXES

- I. ILLUSTRATIONS
- II. TABLES
- III. INSTRUMENTATION

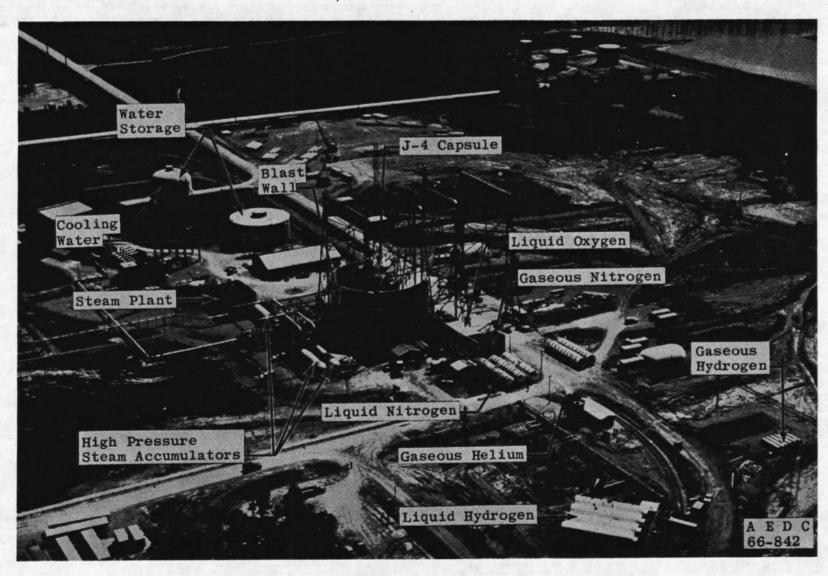


Fig. 1 Test Cell J-4 Complex

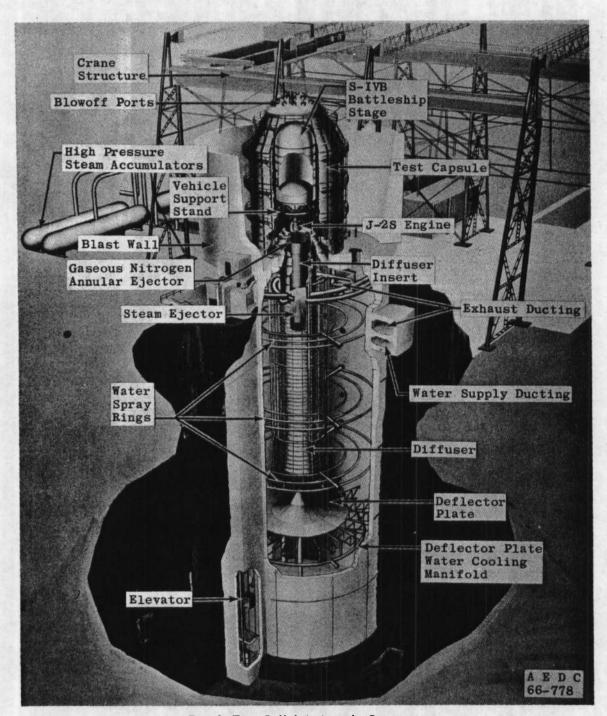


Fig. 2 Test Cell J-4, Artist's Conception

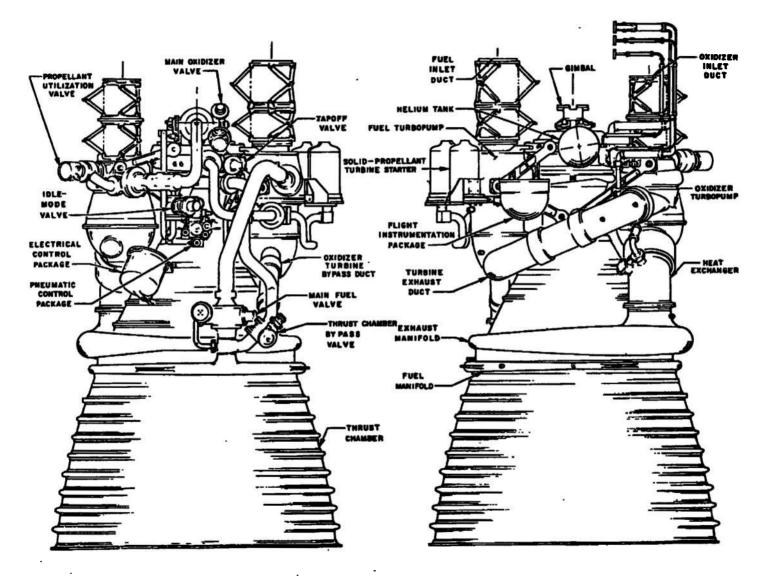


Fig. 3 J-25 Engine General Arrangement

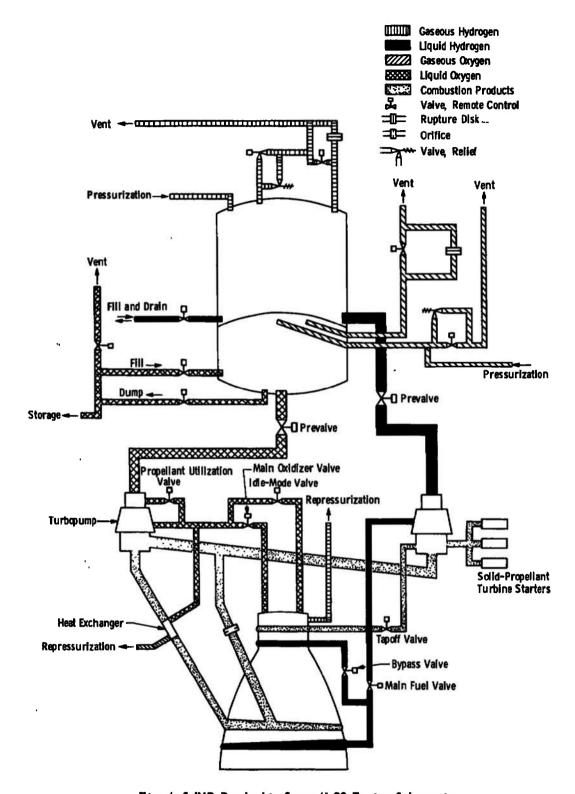
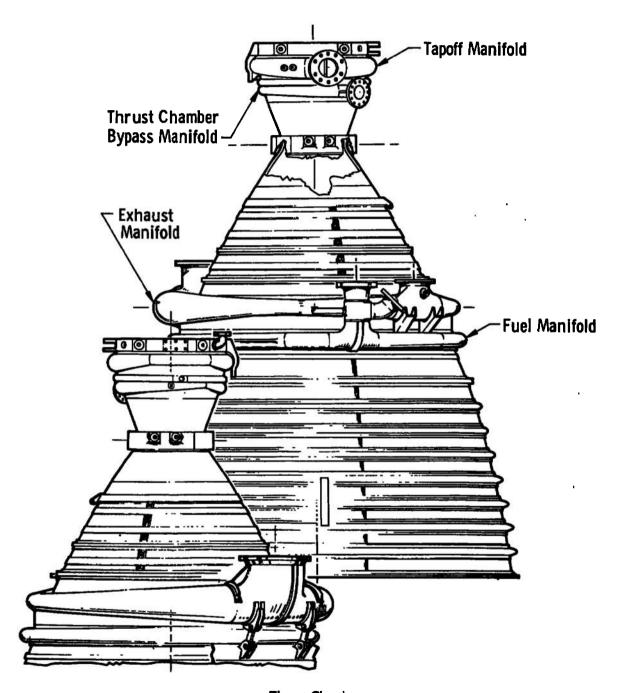
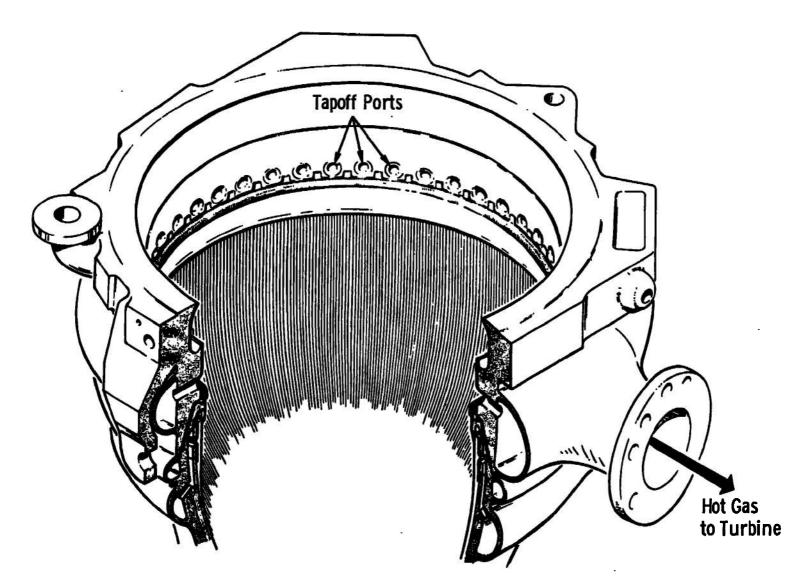


Fig. 4 S-IVB Battleship Stage/J-2S Engine Schematic



a. Thrust Chamber

Fig. 5 Engine Details



b. Combustion Chamber Fig. 5 Continued

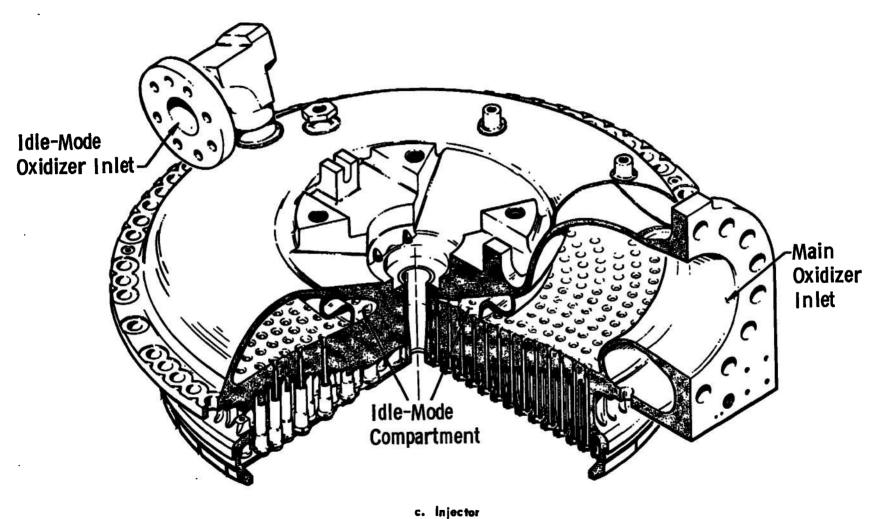
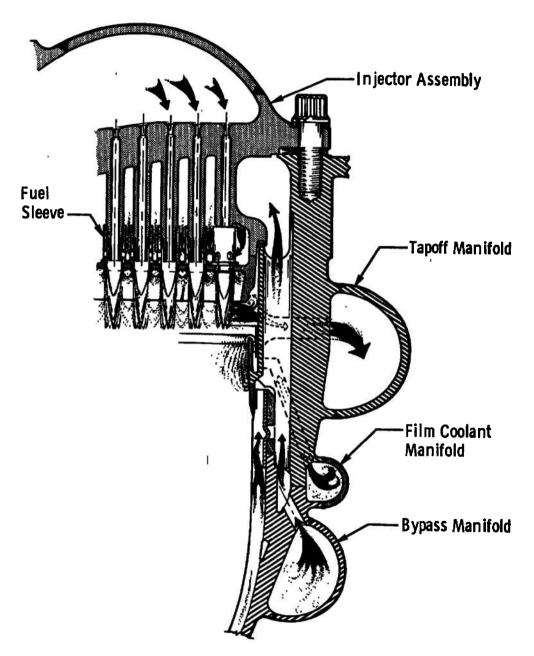


Fig. 5 Continued



d. Injector to Chamber Fig. 5 Concluded

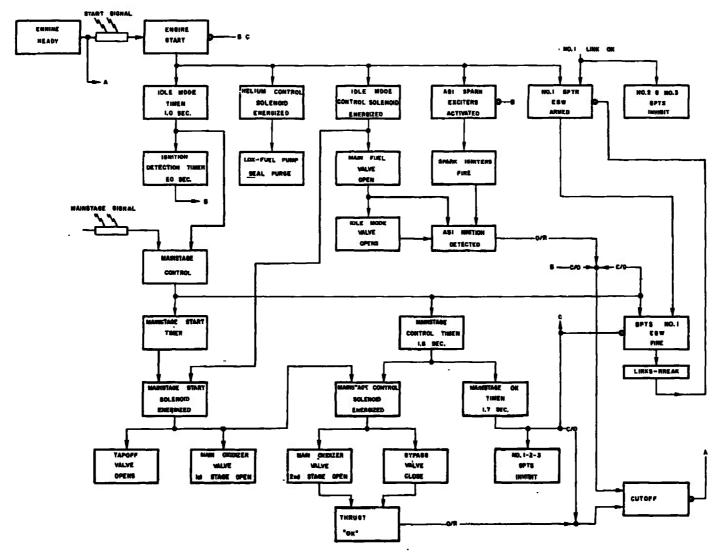
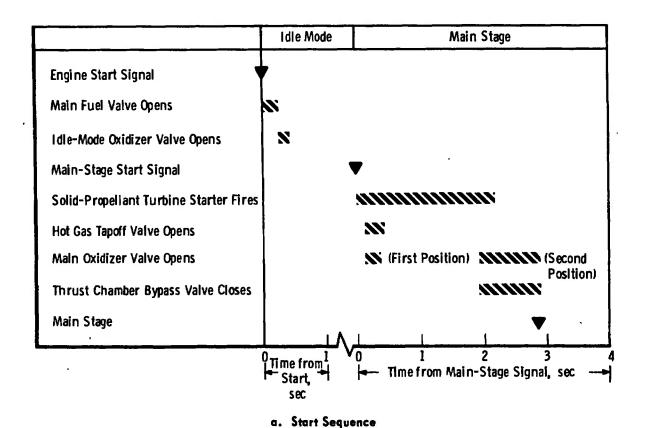
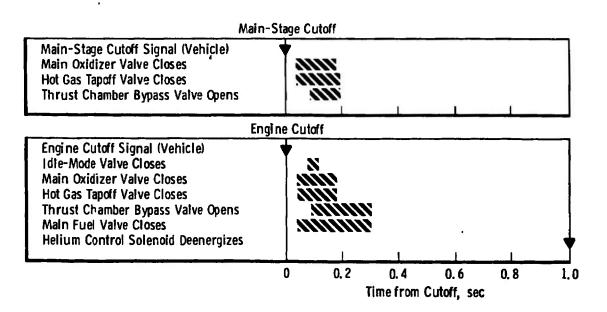


Fig. 6 Engine Start Logic Schematic





b. Shutdown Sequence
Fig. 7 Engine Start and Shutdown Sequence

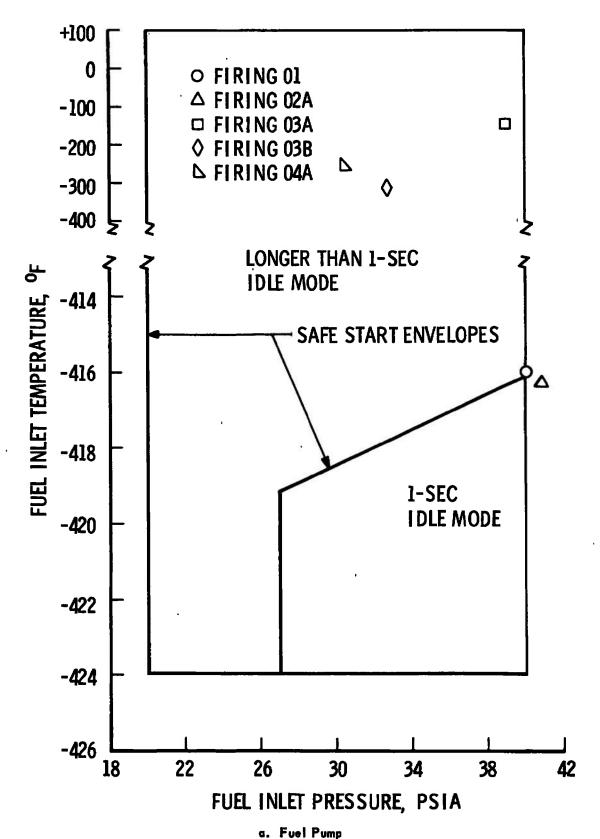
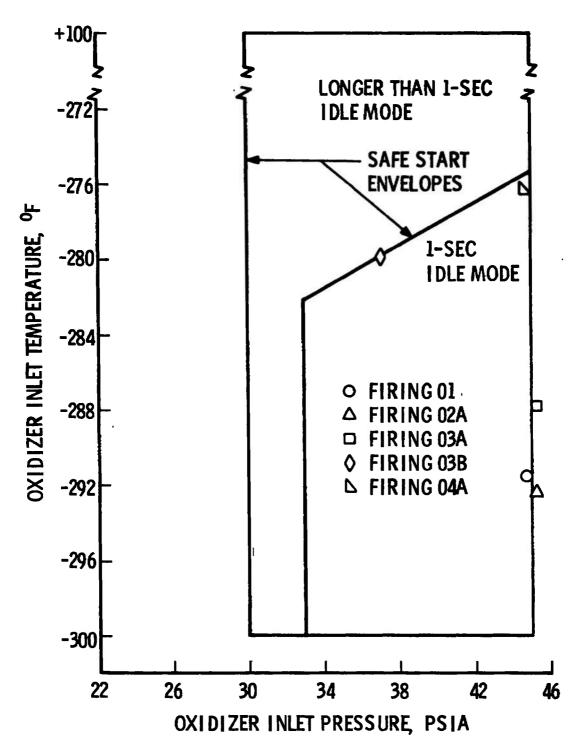


Fig. 8 Engine Start Conditions for Propellant Pump Inlets and Helium Tank



-b. Oxidizer Pump Fig. 8 Continued



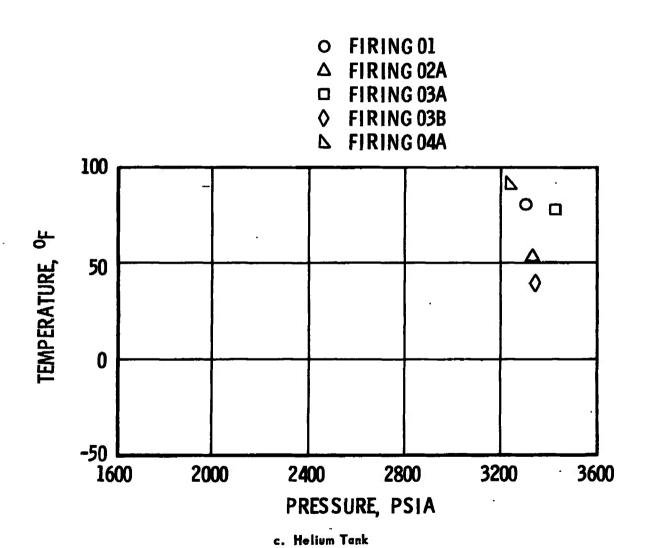


Fig. 8 Concluded

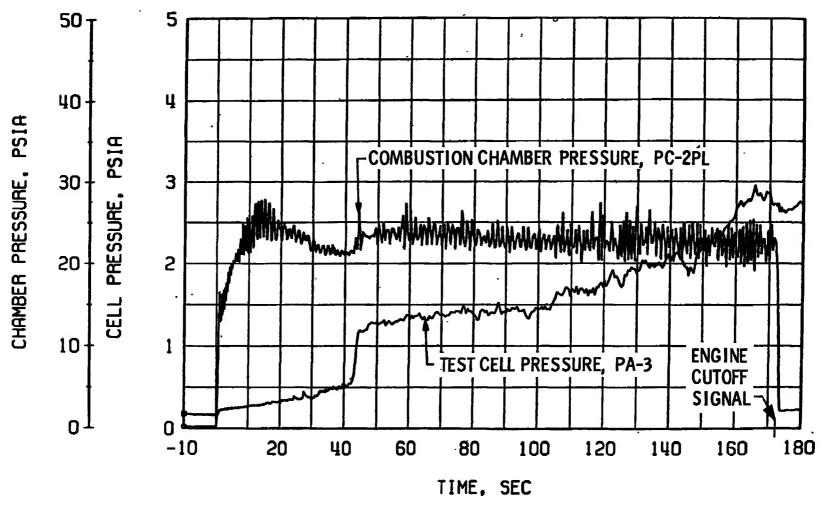


Fig. 9 Engine Ambient and Combustion Chamber Pressure, Firing 01A

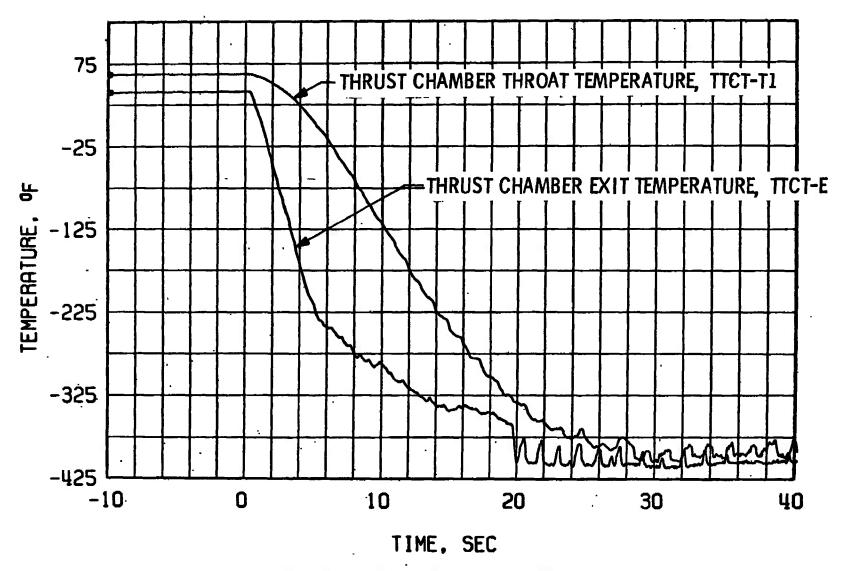


Fig. 10 Thrust Chamber Chilldown, Firing 01A

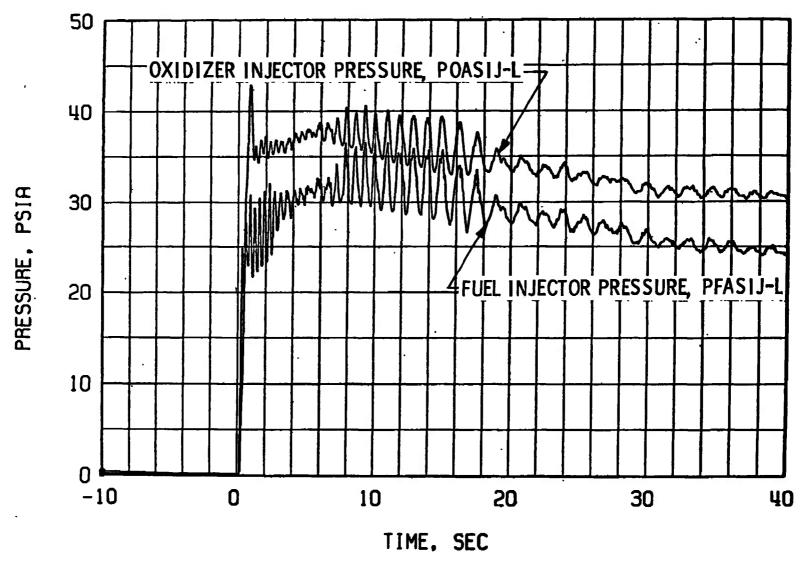
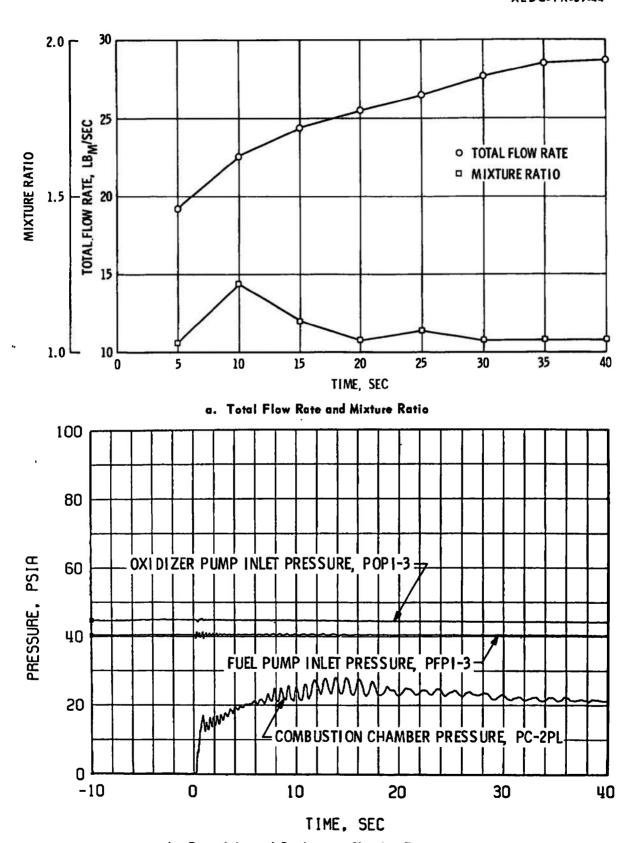


Fig. 11 Augmented Spark Igniter Performance, Firing 01A



b. Pump Inlet and Combustion Chamber Pressures
Fig. 12 Propellant System Performance during Idle Mode, Firing 01A

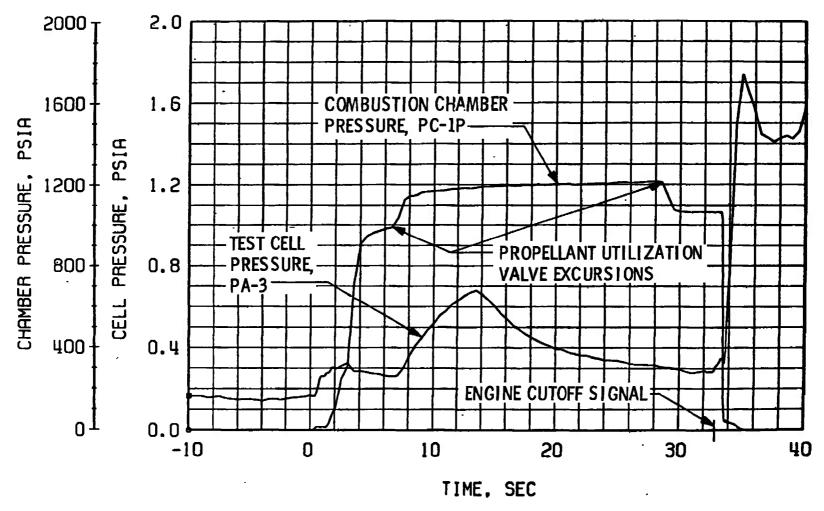
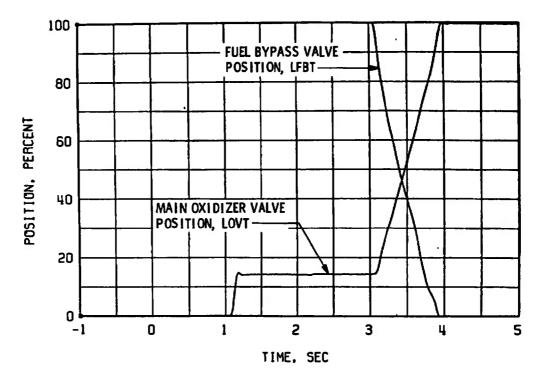
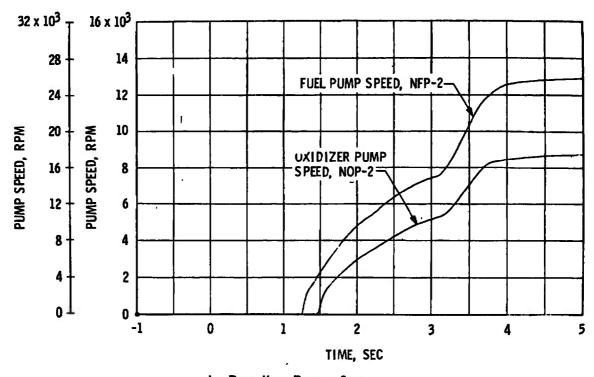


Fig. 13 Engine Ambient and Combustion Chamber Pressure, Firing 02A

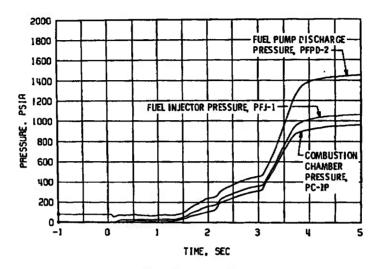


a. Main Oxidizer and Fuel Bypass Valves, Start

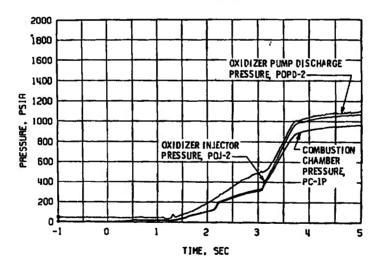


b. Propellant Pumps, Start
Fig. 14 Engine Transient Operation, Firing 02A

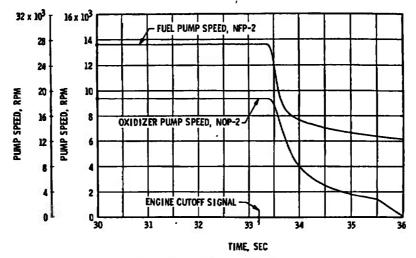
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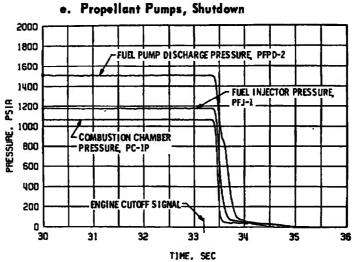


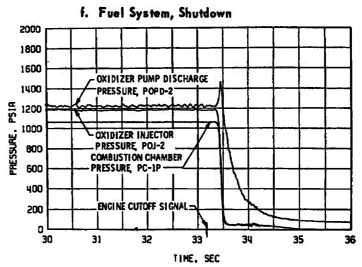
# c. Fuel System, Start



d. Oxidizer System, Start Fig. 14 Continued

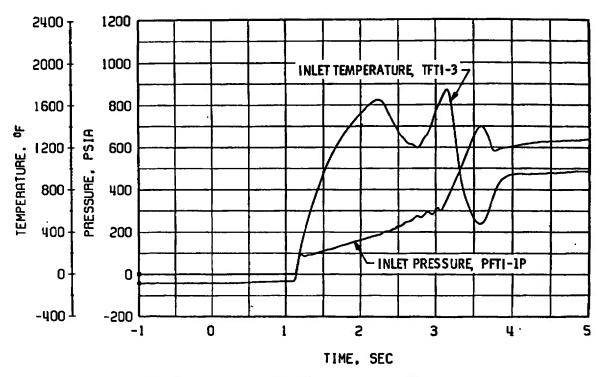




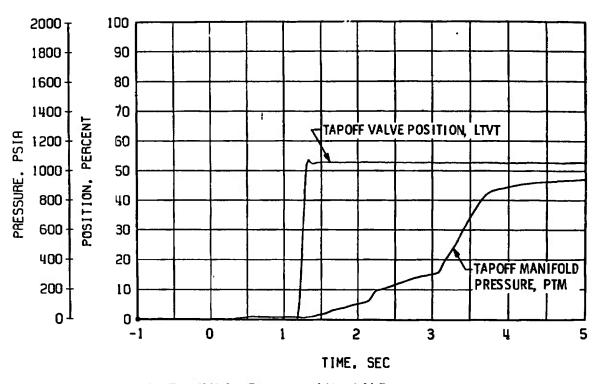


g. Oxidizer System, Shutdown
Fig. 14 Concluded

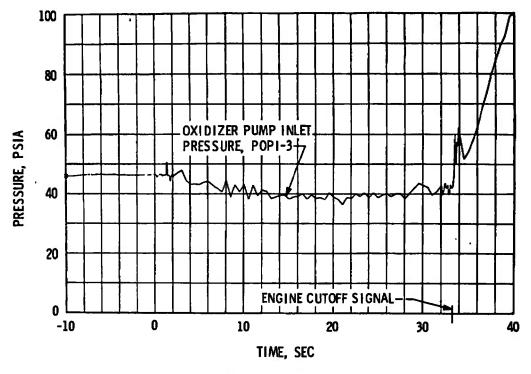
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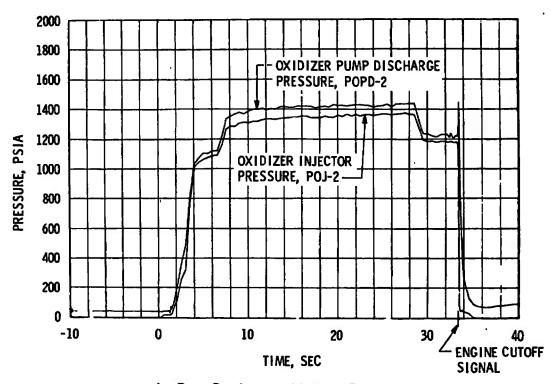
# a. Fuel and Turbine Inlet Temperature and Pressure



b. Tapoff Volve Position and Manifold Pressure
Fig. 15 | Solid-Propellant Turbine Starter Performance, Firing 02A



# a. Pump Inlet Pressure



b. Pump Discharge and Injector Pressure
Fig. 16 Oxidizer System Pressures, Firing 02A

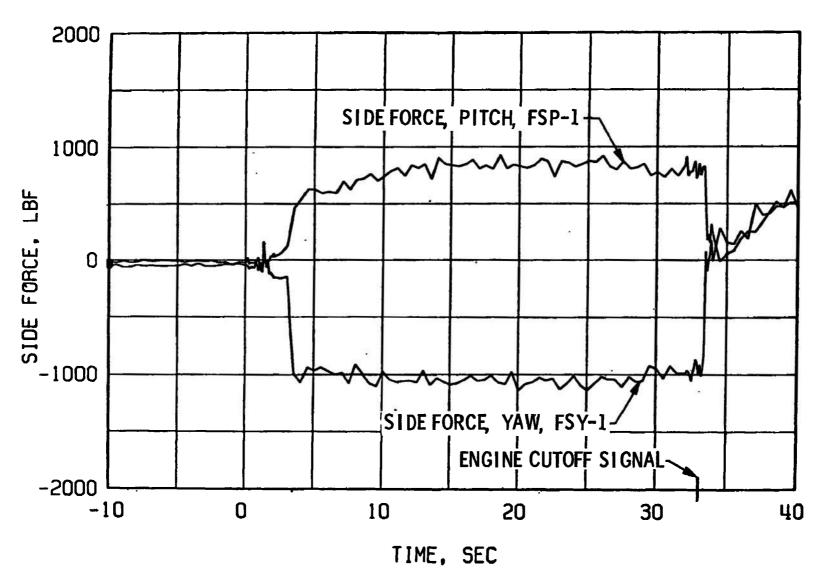


Fig. 17 Engine-Generated Side Loads, Firing 02A

28, 000 RPM

 $60 \times 10^3$ 

NOTE: THE TEST DATA PLOTTED ARE PUMP DISCHARGE STATIC PRES-

SURE CONVERTED TO HEAD.

Fig. 18 Fuel Pump Start Transient Performance, Firing 02A

FLOW, QF-2. GPM

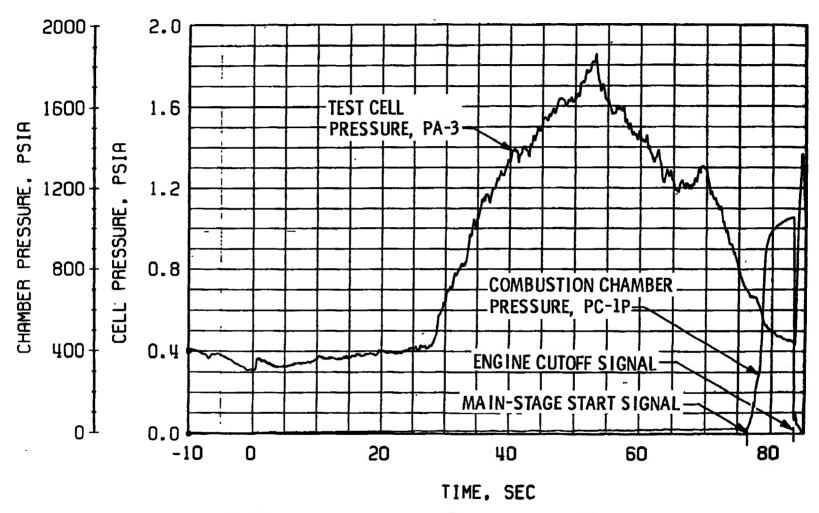


Fig. 19 Engine Ambient and Combustion Chamber Pressure, Firing 03A

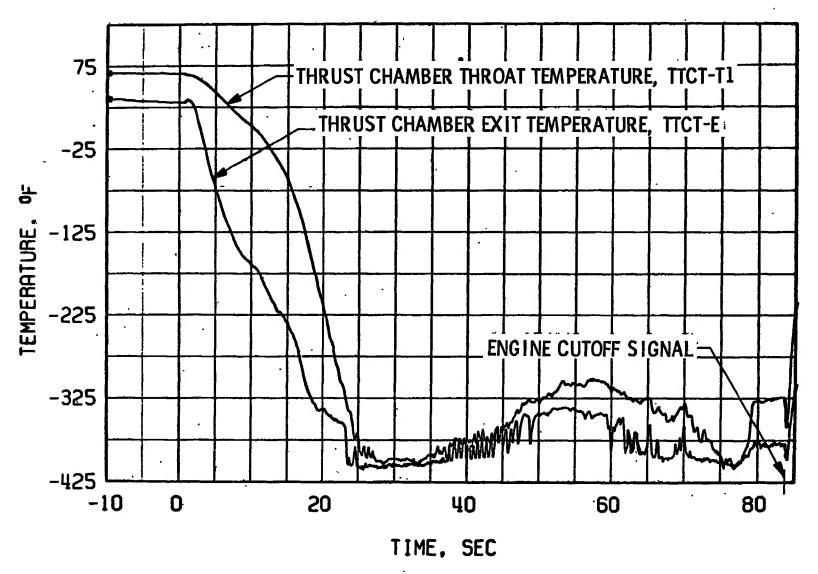


Fig. 20 Thrust Chamber Chilldown, Firing 03A

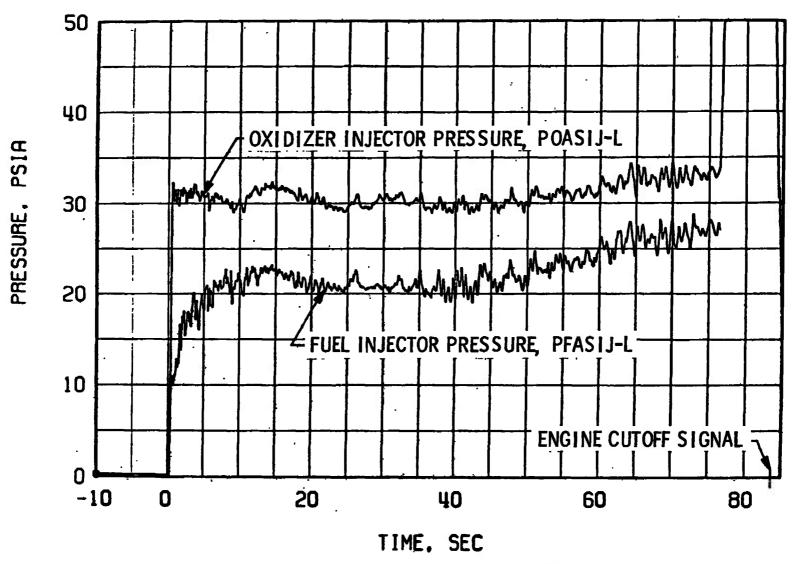
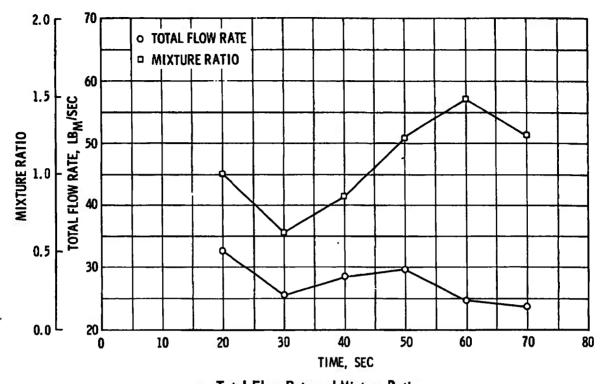
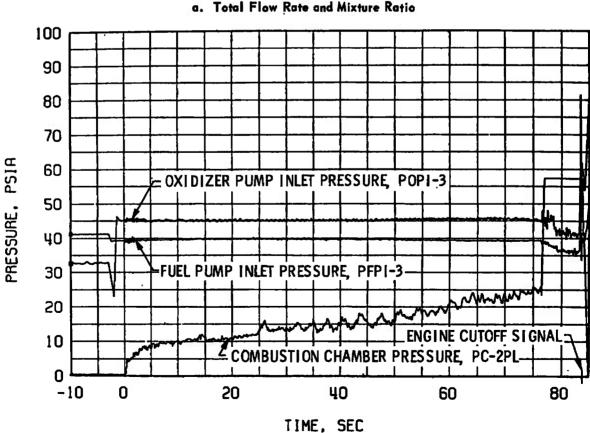
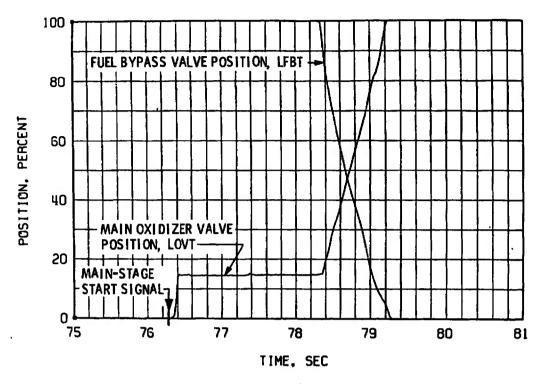


Fig. 21 Augmented Spark Igniter Performance, Firing 03A

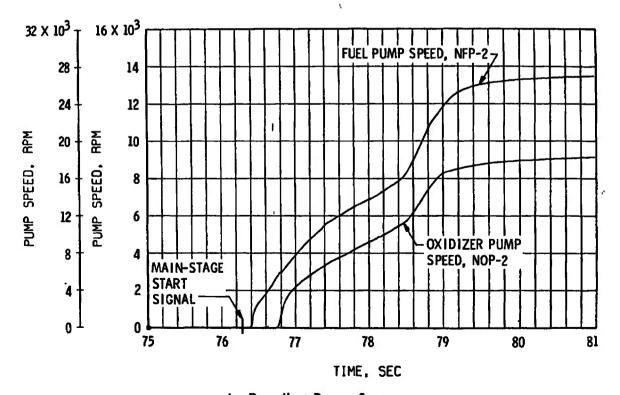




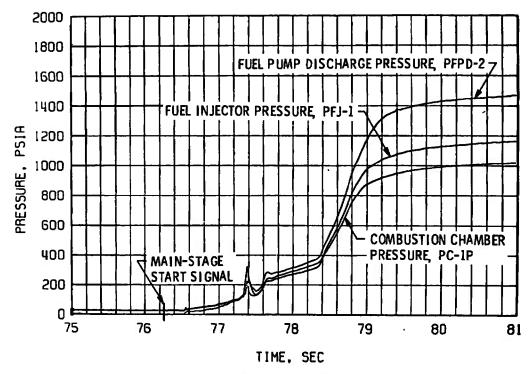
b. Pump Inlet and Combustian Chamber Pressures
 Fig. 22 Propellant System Performance during Idle Mode, Firing 03A



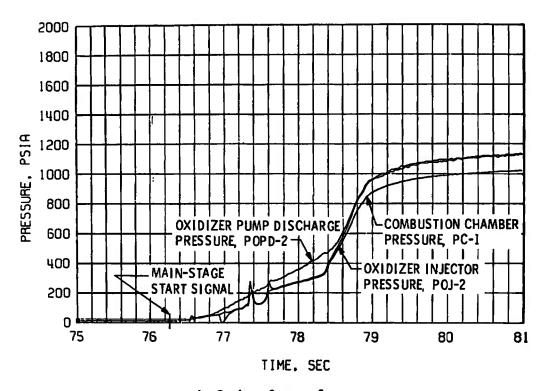
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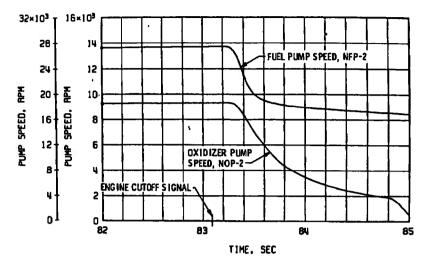
b. Propellant Pumps, Start
Fig. 23 Engine Transient Operation, Firing 03A



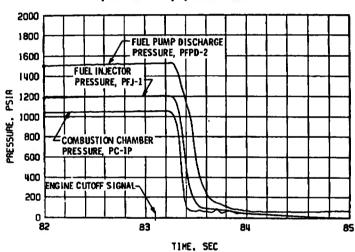
c. Fuel System, Start



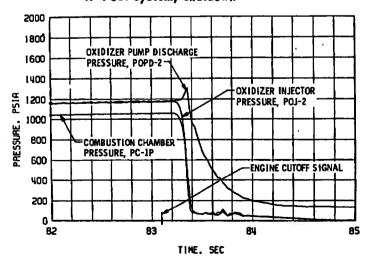
d. Oxidizer System, Start Fig. 23 Continued



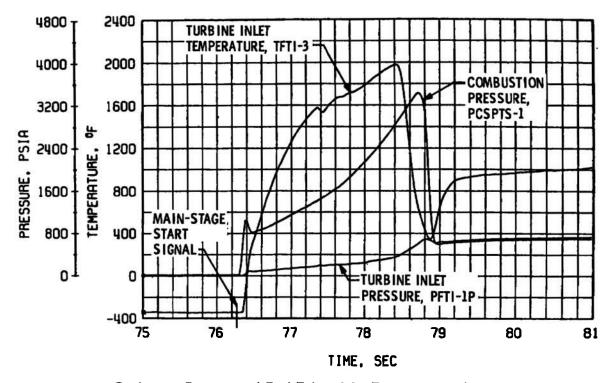
. Propellant Pumps, Shutdown



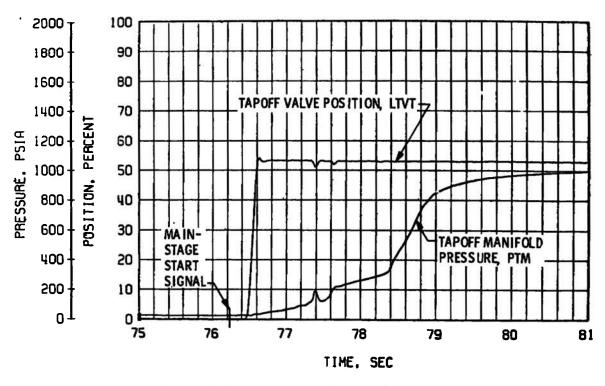
f. Fuel System, Shutdown



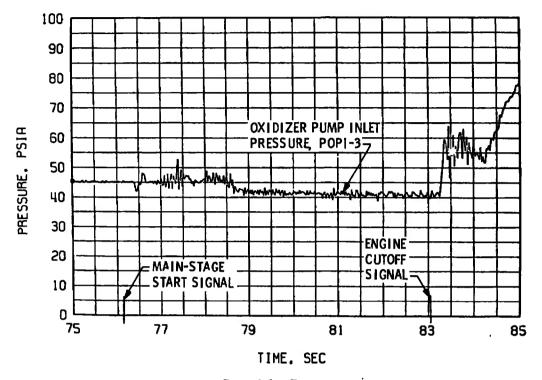
g. Oxidizer System, Shutdown Fig. 23 Concluded



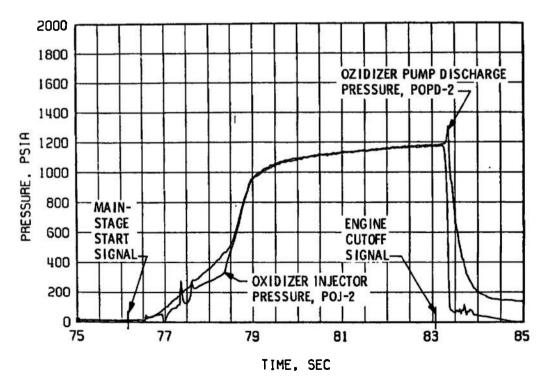
# a. Combustion Pressure and Fuel Tubine Inlet Temperature and Pressure



b. Tapoff Valve Position and Manifold Pressure
Fig. 24 Solid-Propellant Turbine Starter Performance, Firing 03A







b. Pump Discharge and Injector Pressure Fig. 25 Oxidizer System Pressures, Firing 03A

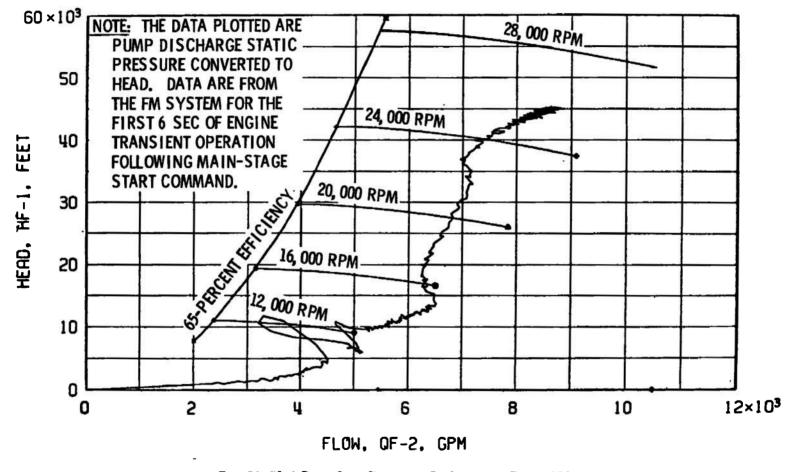


Fig. 26 Fuel Pump Start Transient Performance, Firing 03A

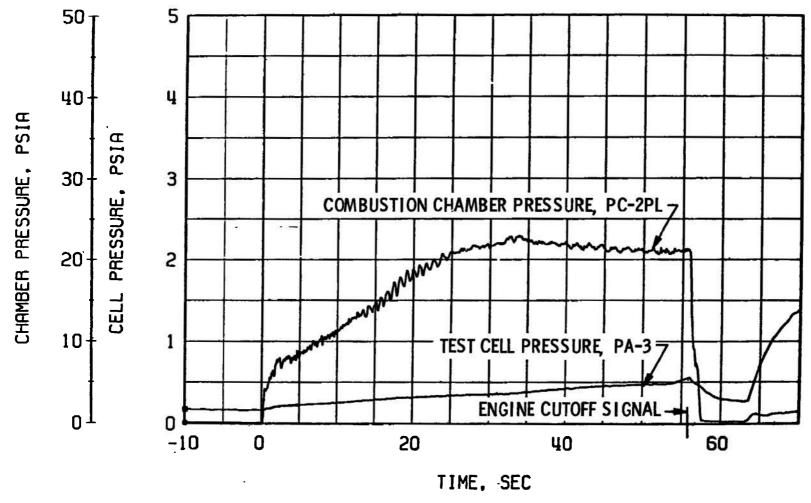


Fig. 27 Engine Ambient and Combustion Chamber Pressure, Firing 03B

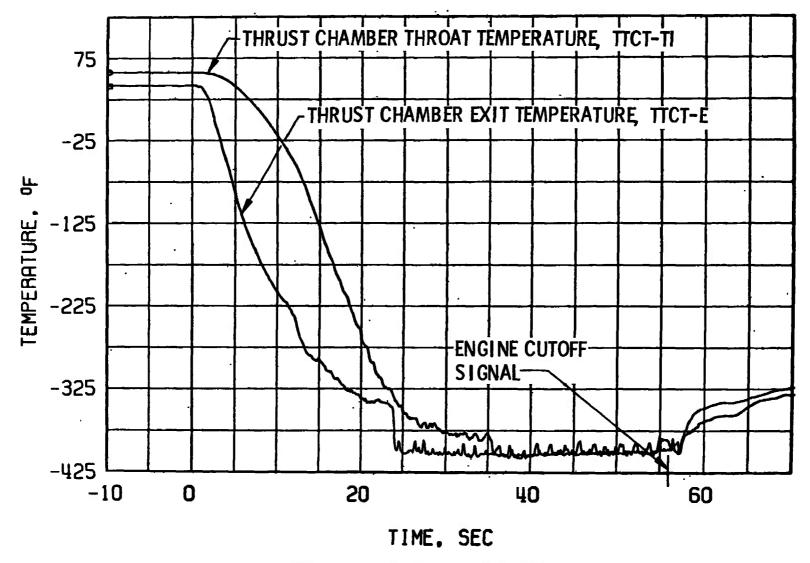


Fig. 28 Thrust Chamber Childown, Firing 03B

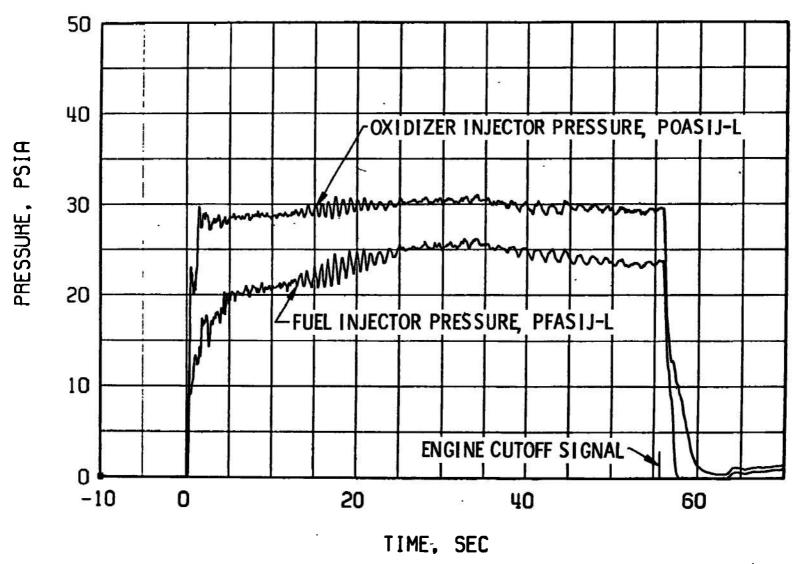
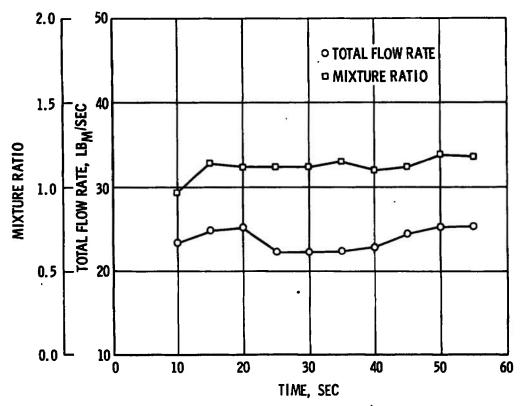
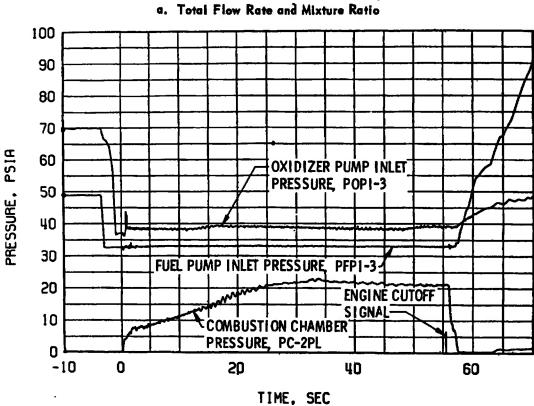


Fig. 29 Augmented Spark Igniter Performance, Firing 03B





b. Pump Inlet and Combustion Chamber Pressure
Fig. 30 Propellant System Performance during Idle Mode, Firing 03B

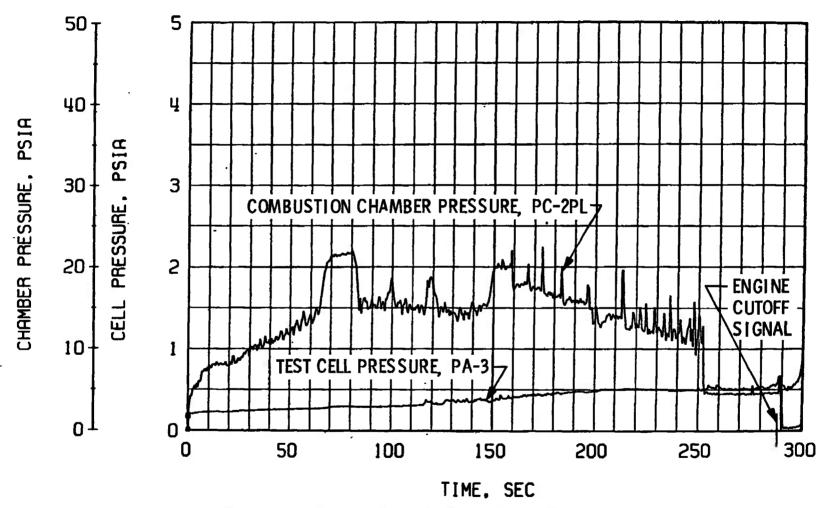
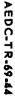


Fig. 31 Engine Ambient and Combustion Chamber Pressure, Firing 04A



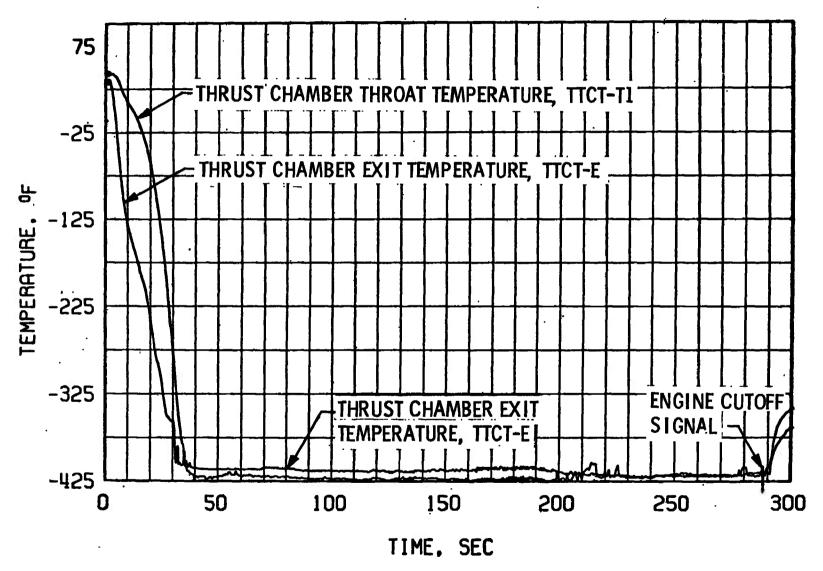


Fig. 32 Thrust Chamber Chilldown, Firing 04A

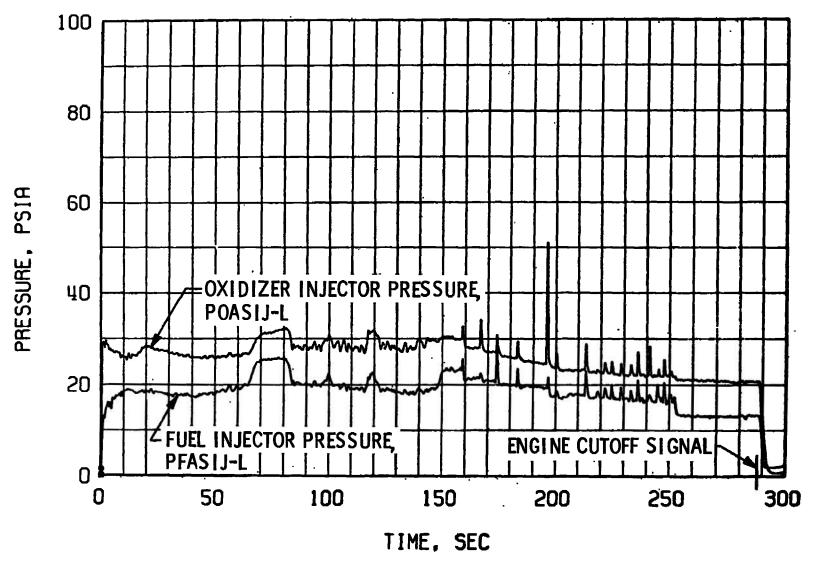
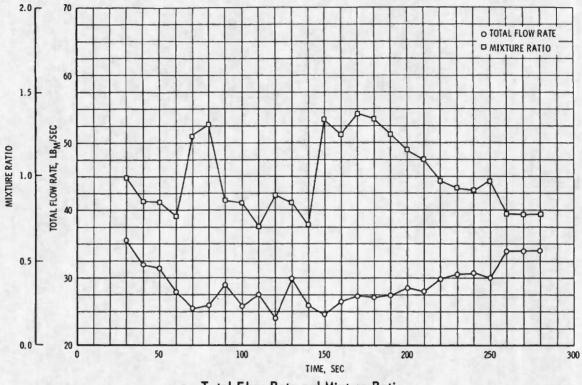
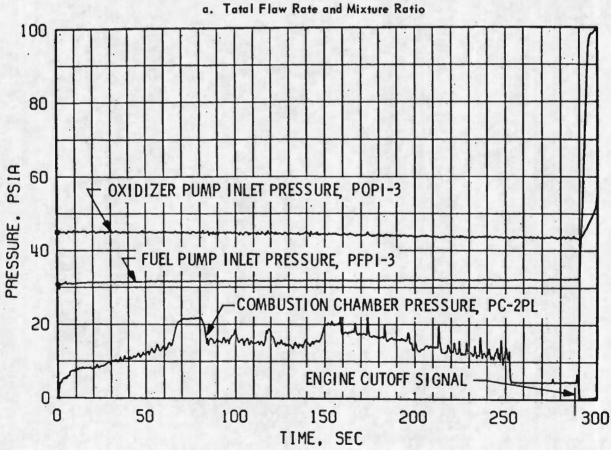
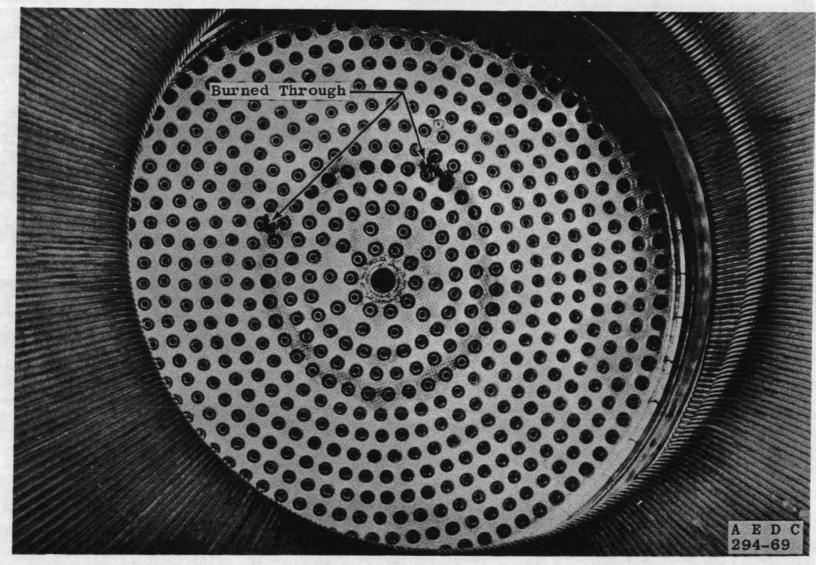


Fig. 33 Augmented Spark Igniter Performance, Firing 04A



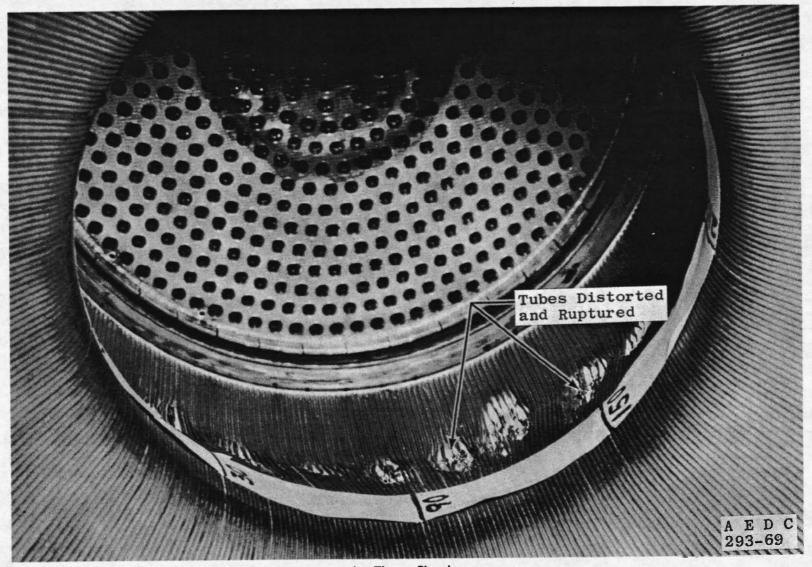


b. Pump Inlet and Combustian Chamber Pressures
Fig. 34 Prapellant System Perfarmance during Idle Made, Firing 04A

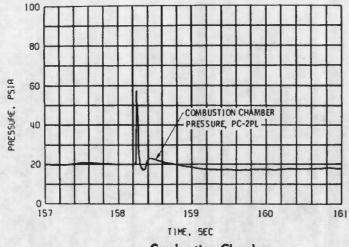


a. Injector

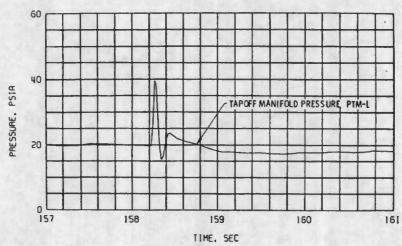
Fig. 35 Engine Damage, Firing 04A



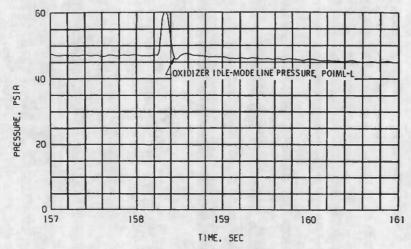
b. Thrust Chamber Fig. 35 Concluded



# a. Combustion Chamber

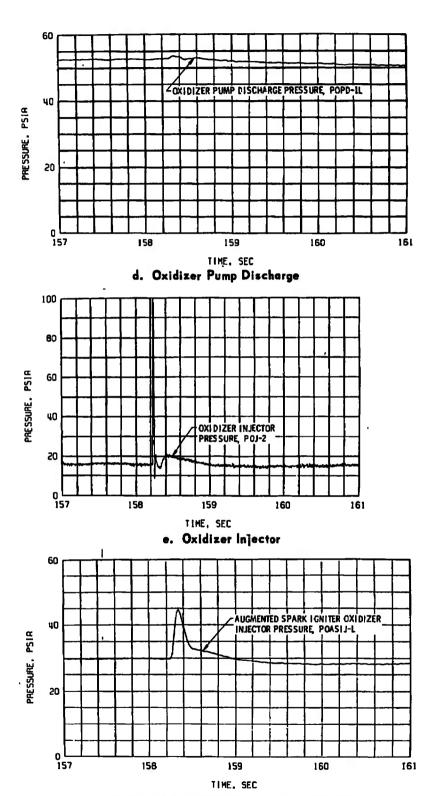


# b. Tapoff Manifold

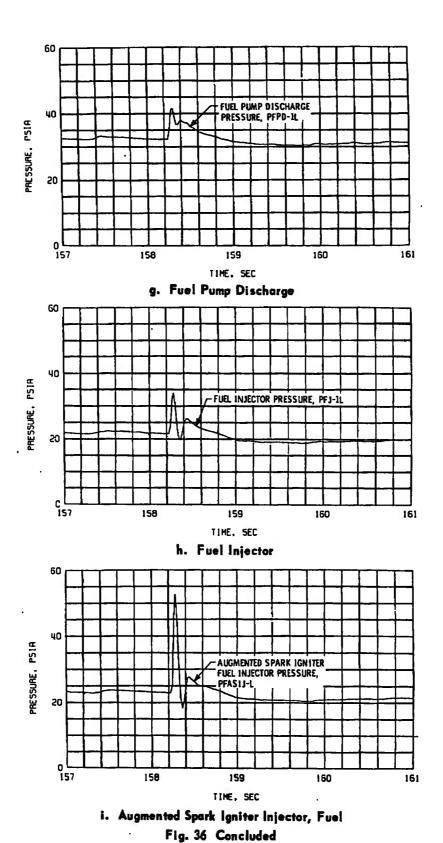


c. Oxidizer Idle-Mode Line

Fig. 36 Pressure Perturbations, Firing 04A



f. Augmented Spark Igniter Injector, Oxidizer
Fig. 36 Continued



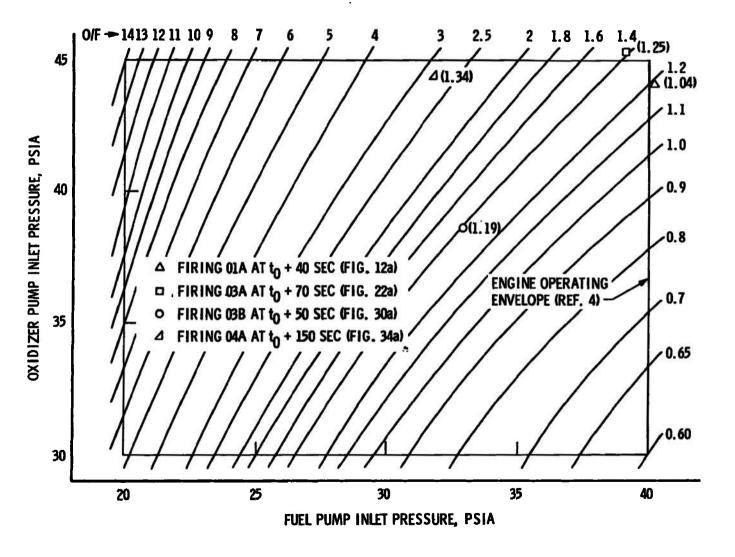
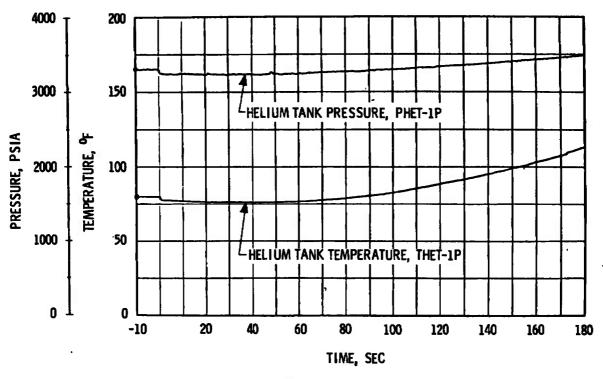


Fig. 37 Idle-Mode Mixture Ratio, Predicted and Measured





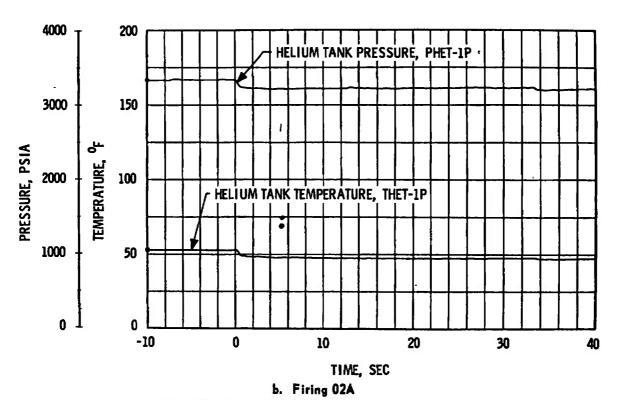
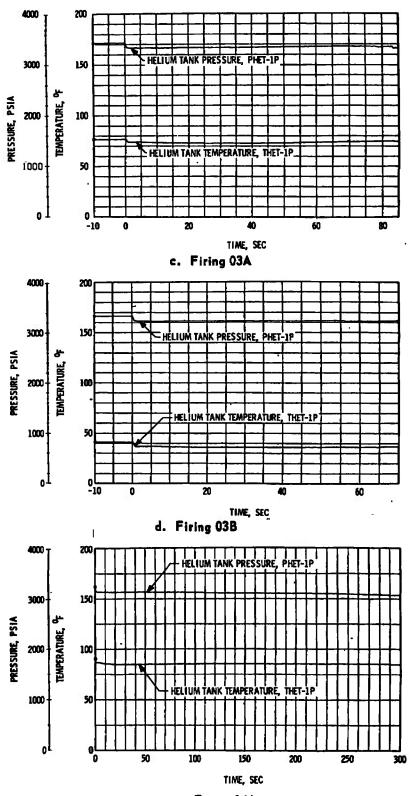


Fig. 38 Helium Tank Pressures and Temperatures



e. Firing 04A Fig. 38 Concluded

TABLE I
. MAJOR ENGINE COMPONENTS
(EFFECTIVE TEST J4-1902-01)

Part Name	P/N	S/N
Thrust Chamber Body Assembly Thrust Chamber Injector	99-210620	4094417
Assembly	99-210610-71	4087379
Augmented Spark Igniter Assembly	652050	4097350
Ignition Detector Probe No. 1	3243-2	041
Ignition Detector Probe No. 2	500750	7202262
Fuel Turbopump Assembly	99-461500	R001-0B
Oxidizer Turbopump Assembly	99-460430	S001-0
Main Fuel Valve	99-411320x3	8900881
Main Oxidizer Valve	99-411225	8900815
Idle-Mode Valve	99-411385	8900816
Thrust Chamber Bypass Valve	99-411180	8900806
Hot Gas Tapoff Valve	99-557824x2	8900847
Propellant Utilization Valve	99-251455x5	8900911
Electrical Control Package	99-503670	4098176
Engine Instrumentation Package	99-704641	4097437
Pneumatic Control Package	99-558330	8900817
Restart Control Assembly	99-503680	4097867
Helium Tank Assembly	80097-1	0002
Oxidizer Flowmeter	251216	4096874
Fuel Flowmeter	251225	4096875
Fuel Inlet Duct Assembly	409900-11	6631788
Oxidizer Inlet Duct Assembly	409899-11	4052289
Fuel Pump Discharge Duct	99-411078	417
Oxidizer Pump Discharge Duct	99-411077	417
Thrust Chamber Bypass Duct	99-411079	417
Fuel Turbine Exhaust Bypass Duct	307879-11	02143580
Hot Gas Tapoff Duct	99-411080-51	7239769
Solid-Fropellant Turbine		
Starters Manifold	99-210921	7216433
Heat Exchanger and Oxidizer		
Turbine Exhaust Duct	307887	2142922
Crossover Duct	307879-11	02143580

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TABLE II
SUMMARY OF ENGINE ORIFICES

Orifice Name	Part Number	Diameter, Inches Unless Otherwise Noted	Test Effective	Comments
Oxidizer Turbine Bypass Nozzle	99-210924	1. 960	J4-1902-01	
Main Oxidizer Valve Closing Control Line	99-411279	0. 0443 208. 5 scfm	J4-1902-01 J4-1902-02	Thermostatic Orifices
Augmented Spark Igniter Oxidizer Supply Line	99-558365-87	0.100	J4-1902-01	
Augmented Spark Igniter Fuel Supply Line				No Orifice Installed

# TABLE III ENGINE MODIFICATIONS (BETWEEN TESTS J4-1902-01 AND J4-1902-04)

34 320 - 42	10. 14.	Description								
Modification	Completion	Description of								
Number	Date	Modification								
Pre-Test										
R 086729	12/3/68	Insulation of Fuel Film Coolant Line and the Augmented Spark Igniter Fuel Line								
T	est J4-1902-01	12/5/68								
R 121031	12/16/68	Replaced Main Oxidizer Valve Closing Control Orifice, 208.5 scfm (Thermostatic Orifice)								
T	est J4-1902-02	12/18/68								
R 121114	12/30/68	Installed Fuel Pump Volute Seal Drain Line								
Test J4-1902-03 1/3/69										
	None									
T	Test J4-1902-04 1/10/69									

# TABLE IV ENGINE COMPONENT REPLACEMENTS (BETWEEN TESTS J4-1902-01 AND J4-1902-04)

Replacement	Completion Date	Component Replaced			
Tes	st J4-1902-01	12/5/68			
P/N 557755-11 S/N 2137550	12/16/68	Oxidizer Idle-Mode Line Purge Check Valve, P/N 557755-11 S/N 2137547			
P/N 99-411225X4 S/N 8900929	12/16/68	Main Oxidizer Valve, P/N 99-411225 S/N 8900815			
Tes	st J4-1902-02	12/18/68			
	None				
Ter	st J4-1902-03	1/3/69			
P/N 554175 S/N 7224310	1/7/69	Oxidizer Dome Purge Check Valve, P/N 554175 S/N 2138996			
Te	st J4-1902-04	1/10/69			

TABLE V . ENGINE PURGE AND COMPONENT CONDITIONING SEQUENCE

Purge	Requirement	Sold Property	et of a	ropelled Drop	ndine sport	Coa Per Cytet	iod &	, et et e	Caped Fried
Oxidizer Dome and Idle-Mode Compartment	Nitrogen, 600 ± 25 psia; 100 to 200°F at /CCP 150 scfm(s)								15 min
Thrust Chamber Jackst, Film Coolant and Turbopump Purges	Helium, 150 ± 25 psia; 100 to 150°F at CCP (125 scfm)		(b) (c)		(a)	15 min (b) (	e) /////	(a)	15 min
Solid-Propeliant Turbine 'Starter Conditioning	Nitrogen, -50 to +140°F	//////////////No. 1, 2	//////// , and 3///			l Remaining Solid-Prope Turbine Starter Install	ellant////////ed		
Main Fuel Valve Conditioning	Helium, -300°F to Ambient			V// <u>*</u> ///					
(a) Engine-Supplied L (b) Any Time Facility (c) 30 min before Pro (d) Initiate Main Fuel (e) 100 to 150°F for F	Water On pellant Drop Valve Conditioning				se Firings with	n Temperature Requir	ements		

TABLE VI SUMMARY OF TEST REQUIREMENTS AND RESULTS

		J4-190	2-01A		02 - 02A	J4-19	02-03A	J4-190	02-03B	J4-190	2-04A
Firing Number		Terget	Actual	Terget	Antuel	Terget	Actual	Taiget	Actual	Target	Aetual
Ftring Date/Time of Day			12/5/68 16/2 hr		12/18/68 2026 hr		1/3/69 1449 hr		1/3/69 1931 hr		1/10/69 1416 hr
Preceure Altitude at to, ft (Ref. 1)	-	100,000	99,000	100,000	99,000	100, 000	86, 000	100,000	101,000	100, 000	98,000
Idle-Mode Duration Pre-Main Stage	, eccO	200	172, 310	1.0	0.996	80	76, 243	100	55, 758	200 Minimum	288. 542
Main-Stage Duration, secO	.03			32, 5	32, 242	7. 5	f. 852				
ldle-Mode Duretion Post-Main Steg	e, sec			<u>/</u>					•		
Fuel Pump Inlet Pressure at to, ps		40.0 ± 1,0	40, 1	40. 0 +1. 0	40. 9	40.0 ± 1.0	39. 0	33, 0 ± 1, 0	32, 8	30,0 ± 1,0	30. 4
Fuel Pump iniet Tempereture et to-	*F		-416.0		-416.6		- 147, 7		-311.4		-255. 8
Fuel Tank Bulk Temperatura at to.	•F	-422, 4 ± 0, 4	- 422.5	-422. 4 ± 0. 4	-422, 4	-422, 4 ± 0, 4	-422.6	-422.4 ± 0.4	-422, 3	-422, 4 ± 0, 4	-422, 6
Oxidizer Pump Inlet Preseure et to	psle _	45.0 ± 1.0	44.7	45.0 ± 1.0	45, 2	45.0 ± 1.0	45. 2	39.0 ± 1.0	37, 1	45.0 ± 1.0	44.7
Oxidizer Pump Inlet Temperature a	t t <sub>0</sub> , *F		-291.8		-292, 4		-287.8		-279.8		-278. 3
Oxidizer Tank Bulk Temperature at to, "F		-295,0±0.4	- 295, 1	-295, 0 ± 0, 4	-295.6	-295, 0 ± 0. 4	-295. 3	-295.0 ± 0.4	-295. 3	-295, 0 ± 0, 4	- 295. 0
elium Tank Conditions et to		3450 -200	3302	3450 ±000	3333	3450 +0 -200	3427	3450 -200	3329	3450 ±0	3240
	Temperature, *F		+80		+53	n •-•	+77		+41		+90
Main Fuel Velve Tempereture et to	•F	•	+96	-100 <sup>+0</sup>	-146		+94		+76		+104
Augmented Sperk Igniter Ignition De	tected, sec (Ref. t <sub>0</sub> )		0, 364		0, 425		0, 481		0, 371		0.412
Propellant Utilization Valve Positio	n et t <sub>0</sub>	Null	Null	Null	Nul1	Null	Null	Nul1	Null	Null	Null
Propellant Utilizetion Velve Excurs	ion, Poeition/Time		/	10 + 6.0	Closed t <sub>0</sub> + 7.0		-:-			-:-	
				Null 10 + 27.5	Null 10+28,5						
	Part Number	•••	•••		99803527-11		89803527-11				
	Sariel Number	•			RT000001		RT000002		••-		
Solid-Propelleat Turbine Starter	Tempereture at to. *F			+50 ± 10	Not Recovered	+50 ± 10	+44		•••		•
	Burn Time, sec				=		2, 4				
	Maximum Pres- eure, pele			•			3420				•••

O<sub>Data</sub> Reducad from Oscillogrem

#### TABLE VII ENGINE VALVE TIMINGS

					-			10		Ste	rt								
Test J4-1902-	Firing	Mein	Mein Fuel Velve		Idle- Mode Oxidizer Velve		Hot Ges Tapoff Velve		Main Oxidixer Valve First Stage		Main Oxidizsr Valve Second Stege			Thrust Chamber Bypass Valve					
		Time of Opening Signal		Valve Opening Time, see	Time of Opening Signal	Valve Delay Time, sec	Valva Opening Time, aec	Time of Opening Signel	Valve Deley Time, see	Valve Opening Time, eee	Time of Opening Signal	Valva Delay Time, soe	Opening		Valve Delay Time, sec	Valve Opening Time, sec	Tims of Closing Signal	Valve Delay Timo, sec	
01	A	0.0	0, 071	0. 112	0.0	0.200	0.059												
	Firel Sequence	0.0	0.047	0.074	0.0	0, 125	0.044	0.094	0.155	0, 110	0.994	0, 076	0.033	2,890	0. 160	0.520	2. 980	0, 166	0.611
05	A	0.0	0. 053	0.062	0.0	0.130	0.035	0.996	0.170	0. 105	0.996	0.060	0.032	2.870	0.188	0. 877	2, 970	0. 157	0.860
	Final Sequence	0, 0	0. 045	0.067	0.0	0, 122	0.045	0. 992	C. 155	0.110	0.992	0.090	0.040	2, 892	0, 205	0, 822	2, 692	0, 150	0. 925
03	Λ	0.0	0. 053	0,059	0.0	0.124	0.034	76. 243	0.164	0. 124	76. 243	0. 075	0.032	76. 126	0, 180	0.878	78, 129	0.150	0.010
	В	0.0	0.053	0.058	0.0	0. 125	0.033						<u></u>						
	Final Sequence	0,0	0.049	0.071	0.0	0. 129	0, 041	0.992	0.162	0.116	0. 992	0.079	0.039	2. 879	0. 192	0.811	2, 879	0.173	0.782
04	A	0,0	0. 050	0.057	0.0	0, 122	0.044			(						🥳			
	Final Sequence	0.0	0. 050	0. 074	0.0	0. 137	0.043												
	-																		<del>                                     </del>

								S	iutdown							
Tent J4-1902-	Firing	Main Oxidizer Valve		Hot Gas Tepoff Volvs		Mein Fuei Valva			[d]e-Mode Oxidizer Valve			Thrust Chamber Bypsse Valvs				
J4-1502-		Time of Closing Signal	Valva Delay Time, sec	Valve Closing Time, sec	Tima of Closing Signal	Velva Delay Time, eec	Valve Closing Time, sec	Time of Closing Signei	Valva Deley Tune, sec	Valve Closing Time, sec	Time of Closing Signal	Valve Delay Time, sec	Velvo Closing Time, sec		Velve Delay Time, sec	Velvo Opening Tune, sec
01	A							172. 302	0.065	0.245	172. 302	0, 065	0. 137			
	Final Sequence	7.049	0.084	0, 146	7.019	0.094	0.210	7,048	0.069	0. 249	7.049	0. 075	0, 118	7, 049	0. 248	0, 220
02	A	33. 244	0, 069	0.150	33, 244	0.094	0, 225	33. 244	0.090	0, 304	33, 244	0. 084	0, 160	33, 244	0, 264	0.200
	Final Sequence	9,666	0.099	0. 144	9, 668	0.097	0, 179	9.669	0.085	0.237	9.899	0, 077	0, 119	9, 668	0. 238	0. 221
03	A	63.095	0.092	0,146	63, 005	0, 085	0. 220	83, 095	0. 092	0.261	63.095	0.071	0, 112	83. 095	0.281	0.164
	В			-	•			55, 756	0. 070	0.252	55. 756	0.069	0, 151			
	Final Sequence	7.970	0.081	0, 142	7. 870	0.088	0, 217	16. 288	0, 099	0.254	16. 288	0. 067	0, 119	7.670	0. 232	0.219
04	A	•••						286, 547	0. 073	0.258	268. 547	0.071	0, 132		-	
	Final Sequence			•••				8, 134	0.071	0, 254	9.134	0, 070	0.119			

Notes:
1. All veive signel times are referenced to t<sub>0</sub>.
2. Velve delay time is the lime required for initial valve movement after the valve "open" or "closed" solenoid has been anargized.
3. Final sequence check is conducted without propellants and within 12 hr bofors testing.
4. Deta ere reduced from oscillogram.

### APPENDIX III INSTRUMENTATION

The instrumentation for AEDC tests J4-1902-01 through J4-1902-04 is tabulated in Tables III-1 and III-2. The location of selected major engine instrumentation is shown in Fig. III-1.

TABLE III-1
INSTRUMENTATION LIST FOR MAIN-STAGE OPERATION

A EDC Code	Parameter	Tap No	Range	Digital Data Syetem	Magnetic Tape	Oscillo- graph	Strip Chart	Event X-Y Recorder Plotter
	Current		amp					
ICC	Control		0 to 30	×				
IIC	Ignition		0 to 30	×				
	Event							•
EASIS-1	Augmented Spark Igniter No 1 Spark		On/Off					x
EASIS-2	Augmented Spark Igniter No. 2 Spark		On /Off					x
EECL	Engine Cutoff Lockin		On/Off	×		×		x
EECO	Engine Cutoff Signal		On/Off	x		×		×
EER	Engine Ready Signal		On/Off					x
RES	Engine Start Command		On/Off	x		x		×
EESCO	Programmed Duration Cuto	of f	On/Off					×
EFBVO	Fuel Bleed Valve Open Limit		On/Off					*
EFPCO	Fuel Pump Overspeed Cut- off	-	On/Off					×
EFPVC	Fuel Prevalve Closed Liz	nit	On/Off	x	•			x
EFPVO	Fuel Prevalve Open Limit	t	On/Off	x				×
EFUA	Exploding Bridge Wire Firing Units Armed		On/Off					×
EHCS	Helium Control Solenoid Energized		On/Off	x	×	x		x
EHGTC	Hot Gam Tapoff Valve Closed Limit		On/Off					x
EHGTO	Hot Gae Tapoff Valve Open Limit		On/Off					x
EID	Ignition Detected		On/Off	x		×		×
EIDA-1	Ignition Detect Amplific	er	On/Off					x
EIDA-2	Ignition Detect Amplific	er	On/Off					x
EIMCS	Idle-Mode Control Solene Energized	oid	On/Off	×		x		x
EINVC	Idle-Mode Valve Closed !	Limit	On/Off					x x
EIMVO	Idle-Mode Valve Open Lis	n1t	On/Off					x
EMCL	Main-Stage Cutoff Locki	n	On/Off	×		×		×
ENCO	Main-Stage Cutoff Signal	ı	On/Of f	x		×		
ENCS	Main-Stage Control Sole	noi d	On/Off	x		×		x
EMD-1	No. 1 Main-Stage "OK" Depreseurized		On/Off	· x		x		×
EMD-2	No. 2 Main-Stage "OK" Depreseurized		On/Off	×		x		x
EXFVC	Main Fuel Valve Closed	Limit	On/Off					×
EMFVO	Main Fuel Valve Open Lin	nit	On/Off					x
EMOVC	Main Oxidizer Valve Clos Limit	ed	On/Off					ж

#### TABLE III-1 (Continued)

AEDC Code	Parameter	Tap No.	Range	Digital Data System	Magnetic Tape	Oscillo- graph	Strip Chart	Event X-Y Recorder Plotter
	Event							
EMOVO	Main Oxidizer Valve Open Limit		On/Off					×
ENP-1	No. 1 Main-Stage "OK" Pressurized		On/Off	×		×		×
EMP-2	No. 2 Main-Stage "OK" Pressurized		On/Off	x				x
ENPCO	Main-Stage Pressure Cut Signal	off	On/Off					x
EMS	Main-Stage Start Signal		On/Off					x
EMSCO	Main-Stage Programmed Duration Cutoff		On/Off					x
EMSS	Main-Stage Start Soleno Energized	id	On/Off	x	×	×		x
DOSVO	Oxidizer Bleed Valve Open Limit		On/Off					ж .
ECCO	Observer Cutoff Signal		On/Off					×
EOPCO	Oxidizer Pump Overspeed Cutoff Signal		On/Off					×
EOPVC	Oxidizer Prevalve Close	d	On/Off	×				ж
BOPVO	Oxidizer Prevalve Open Limit		On/Off	×				X
EOTCO	Fuel Turbine Overtemper ture Cutoff	-	On/Off					x
eras IS-1	Augmented Spark Igniter No. 1 Spark Rate		On/Off			x		
eras is-2	Augmented Spark Igniter No. 2 Spark Rate		On/Off			×		
ES 1M1	No. 1 Solid-Propellant Turbine Starters Ex- ploding Bridge Wire No. 1 Monitor		On/Off	×		×		
ES1N2	No. 1 Solid-Propellant Turbine Starters Ex- ploding Bridge Wire No. 2 Monitor		On/Off	x		×		,
ES 2 M1	No. 2 Solid-Propellant Turbine Starters Ex- ploding Bridge Wire No. 1 Monitor		On/Off	×		×		
ES2N2	No. 2 Solid-Propellant Turbine Starters Ex- ploding Bridge Wire No. 2 Monitor		On/Off	x		×		
es 3 m1	No. 3 Solid-Propellant Turbine Starters Ex- ploding Bridge Wire No. 1 Monitor		On/Off-	x		ж		
ES3N2	No. 3 Solid-Propellant Turbine Starters Ex- ploding Bridge Wire No. 2 Monitor		On/Off	x		×		
ESANCO	Stall Approach Monitor Cutoff		On/Off					x
ESPTS	Solid-Propellant Turbine Starter Initiated		On/Off					×

TABLE III-1 (Continued)

AEDC Code	Parameter	Tap No.	Range	Digital Data System	Wagnetic Tape	Oscillo- graph	Strip Event X-Y Chart Recorder Plotter
	Event						•
ESR-1	No. 1 Solid-Propellant Turbine Starter Ready		On/Off	×		×	×
ESR-2	No. 2 Solid-Propellant Turbine Starter Ready		On/Off	×		×	×
ESR-3	No. 3 Solid-Propellant Turbine Starter Raady		On/Off	×		×	<b>x</b> .
ESTCO	Start "OK" Timer Cutoff Signal		On/Off				×
ETCBC	Thrust Chamber Bypass Valve Closed		On/Off				×
ETCBO	Thrust Chamber Bypass Valve Open		On/Off				<b>x</b>
EVSC-1	Vibration Safety Counts No. 1		On/Off			×	
EVSC-2	Vibration Safety Counts No. 2		On/Off			×	
EVSC-3	Vibration Safety Counts No. 3		On/Off			x	
	Flows		gpm				
QF-1	Engine Fuel Flow PFF		0 to 11,000	x			
QF-2	Engine Fuel Flow PFF		o to 11,000	×	×	x	
QF-3	Engine Puel Plow PFF	-	0 to 11,000	-	×	×	
QF-1SAM	Fuel Flow Stall Approach Monitor		3 10 11,000	×	-	×	
Q0-1	Engine Oxidizer POF		0 to 3600	×			•
Q0-2	Engine Oxidizer POF	À	0 to 3600	×	×	×	
Q0-3	Engine Oxidizer POF		0 to 3600		×	×	
	Forces		1bf				
PSP-1	Side Load (Pitch)		±20,000	×		×	
FSY-1	Side Load (Yaw)		±20,000	×		×	
	<u>Position</u>		Percent Open				
LFBT	Thrust Chamber Bypass Valve		0 to 100	×		×	
LFVT	Main Puel Valve		0 to 100	×		×	
LIMT	ldle-Mode/Augmented Spa Igniter Oxidizer Valv		0 to 100	×		×	
LOVT	Main Oxidizer Valve		0 to 100	×		×	
LPUTOP	Propellant Utilization Valve		5 volts	×		×	x
LTVT	Hot Gas Tapoff Valve		0 to 100	x		×	
	Pressure	•	<u>psia</u>				
PA-1	Test Cell		0 to 0.5	×			
PA-2	Test Cell		0 to 1.0	×			`
PA-3	Test Cell		0 to 5.0	x		, <b>x</b>	

TABLE [!!-1 (Continued)

AEDC Code	Parameter	Tap No.		Range	Digital Data System	Magnetic Tape	Oscillo- graph	Strip Chart	Event Recorder	X-Y Plotter
	Preseure			psia						
PC-1P	Thrust Chamber	CG1	0	to 1500	×					
PC-2P	Thrust Chamber	CG1a-2	0	to 1500	×		×	×		
PC-2PL	Thrust Chamber	CG1 a-1	0	to 50	×			×		
PCSPTS-1	Solid-Propellant Turbine Starter No. 1 Chamber	PTS-1	0	to 5000	x		x			
PCS PTS-2	Solid-Propellant Turbine Starter No. 2 Chamber	PTS-2	0	to 5000	×		×			
PCS PTS-3	Solid-Propellant Turbine Starter No. 3 Chamber	PTS-3	0	to 5000	x		x			
PFAS IJ	Augmented Spark Igniter Fuel Injection	CF4	0	to 2000	x					
PPAS I J—L	Augmented Spark Igniter Fuel Injection	CP4	0	to 50	x					
PPBM	Thrust Chamber Bypase Manifold	CF3	0	to 1500	×					
PFCO	Film Coolant Orifice	CF5	0	to 2000	×					
PFCO-L	Film Coolant Orifice	CF5	0	to 50	*					
PFJ-1	Fuel Injection	CF2	0	to 1500	×		×			
PFJ-1L	Fuel Injection	CF2	0	to 50	×					
PPNI	Fuel Jacket Mani- fold Inlet	CF1	0	to 2000	×					
PPMI—L	Fuel Jacket Mani- fold Inlet	CF1	0	to 50	×					
PFPBC	Fuel Pump Balance Piston Cavity	PF5	0	to 2000	×		×	×		
PF PBS	Fuel Pump Balance Piston Sump	PF4	0	to 1000	×		ж	×		
PFPD-1L	Fuel Pump Dis- charge	PF3	0	to 50	×					
PFPD-1P	Fuel Pump Dis- charge	PF3	0	to 2500	<b>*</b>			×		
PFPD-2	Fuel Pump Dis- charge	PF 2	0	to 3000	×	×	×			
PFPI-1	Fuel Pump Inlet	PF1	0	to 100	×			×		×
PFP1-2	Fuel Pump Inlet		0	to 100	×					×
PFP I-3	Fuel Pump Inlet	PFla	0	to 100	×	×	×			x
PFPRB	Fuel Pump Rear Bearing Coolant	PE 7	0	to 1000	×			×		
PFPS	Fuel Pump Inter- stage	PF6		to 1000			×			
PFPS I	Fuel Pump Shroud Inlet			to 2500				×		
PFT I-1P	Fuel Trubine Inlet	TG1		to 1000			×			
PFTO	Fuel Trubine Outlet	'TG2	0	to 200	×		•			

#### TABLE III-1 (Continued)

AEDC Code	Parameter	Tap No.	Range	Digital Data System	Magnetic Tape	Dscillo- graph	Strip	Event Recorder	X_Y Plotter
	Preseure		psia						
PFTSC	Fuel Turbine Seal Cavity	TG10	0 to 500	×					
PFUT	Fuel Ullage Tank		0 to 100	×					
PFVC	Fuel Repressurization at Customer Connect Panel		0 to 2000	x					
PFVI	Fuel Repressurization Nozzle Inlet	KHF1	0 to 2000	×					
PFVL.	Fuel Represeurization Nozzle Throat	KHF2	0 to 1000	x					
PHEA	Helium Accumulator	NN3	0 to 750	×					
PHES	Helium Supply		0 to 5000	×					
PHET-1P	Helium Tank	NN1-1	0 to 5000	×					×
PHET-2P	Helium Tank	NN 1-3	0 to 5000	x					
PHRO-1P	Helium Regulator Outlet	NN2	0 to 750	x					
PNODP	Oxidizer Dome Purge at Cuetomer Connect Pane	1	0 to 750	×					
POASIJ	Augmented Spark Igniter Oxidizer Injection	103	0 to 1500	x		×			
POASIJ-L	Augmented Spark Igniter Oxidizer Injection	103	0 to 50	x					
POINL	Oxidizer Idle-Modo Line	PO10	0 to 2000	×					
POIML-L	Oxidizer Idle-Mode Line	PO10	0 to 50	×					
P0J-1	Oxidizer Injection	CO3	0 to 1500	×					
POJ-2	Oxidizer Injection	C03a	0 to 2000	×		x			
P0J-3	Oxidizer Injection Manifold	СоЗь	0 to 5000		x				
POPBC	Oxidizer Pump Bearing Coolant	P07	0 to 500	×					
POPD-1L	Oxidizer Pump Discharge	P03	0 to 50	×					
POPD-1P	Oxidizer Pump Discharge	P03	0 to 2500	×					
POPD-2	Oxidizer Pump Discharge	P02	0 to 3000	×	×	×			
POPI-1	Oxidizer Pump Inlet	P01	0 to 100	×					×
POPI-2	Oxidizer Pump Inlet		0 to 100	×					×
POPI-3	Oxidizer Pump Inlet	POla	0 to 100	×	×	×		•	
POPSC	Oxidizer Pump Primary Seal Cavity	<b>P</b> 06	0 to 50	x					
POTI-1P	Oxidizer Turbine Inlet	TG3	0 to 200	×					
POTO-1P	Oxidizer Turbine Outlet	TG4	0 to 100	x					
POUT	Oxidizer Ullage Tank		0 to 100	×					
POVC	Oxidizer Repressuriza- tion at Cuetomer Connect Panel		0 to 2000	×					
POVI	Oxidizer Represeuriza- tion Nozzle Inlot	кно1	0 to 1500	×					

TABLE III-1 (Continued)

ARDC Code	<u>Parameter</u>	Tap No.	Range	Digital Data System	Magnetic Tape	Oscillo- graph	Strip Chart	Event L-Y Recorder Flotter
	Preseure		psia					•
POVL	Oxidizer Represeuriza- tion Nozzle Throat	KH02	0 to 1000	×				
PPTD	Photocon Cooling Water (Downetream)		0 to 100	x				
PPTU	Photocon Cooling Water (Upstream)		0 to 100	×				
PPUV I	Propellant Utilization Valve Inlet	PO8	0 to 2000	×				
PPUVO	Propellant Utilization Valve Outlet	P09	0 to 1000	x				
PTCFJP	Thrust Chamber Fuel Jacket Purge		0 to 200	×				
PTEN	Turbine Exhauet Manifold	TG5	0 to 50	x				•
PTM	Tapoff Manifold	GG25	0 to 1500	×				
PTM-L	Tapoff Manifold	GGZb	0 to 50	×				
	Speeds		rpm					
NFP-1	Fuel Pump	PPY	0 to 33000		×			
NFP-2	Fuel Pump	PPY	0 to 33000	×		×		
NFP-3	Fuel Pump	PPV	0 to 33000			×		
NOP-1	Oxidizer Pump	POV	0 to 12000		×			
NOP-2	Oxidizer Pump	POV	0 to 12000	×		×		
NOP-3	Oxidizer Pump	POY	0 to 12000			×		
			••					
	Temperatures		<u>*7</u>	_				
TA-1 TA-2	Test Cell North		-50 to 800	×				
TA-3	Teet Cell East		-50 to 800	×				
TA-4	Teet Cell South Teet Cell West		-50 to 800	x x				
TECP-1P	Electrical Control	NST1a	_300 to 200					
TFAS IJ	Ascembly Augmented Spark Igniter		-425 to 100			×		
12 80 10	Fuel Injection		,	^		•		
TFD-Avg	Fire Detection Average		0 to 1000	×			x	
TEDETA	Fire Detect Fuel Turbin Manifold Area	16	0 to 500	x				
TPDMFVA	Fire Detect Main Fuel Valve Area		0 to 500	x				
TPDMOVA	Fire Detect Main Oxidia Valve Area	ter	0 to 500	×				
TFDODA	Fire Detect Oxidizer Done Area		0 to 500	×				
TFDTDA	Fire Detect Tapoff Duct Area		0 to 500	×				
TFJ-1P	Fuel Injection	CFT2	-425 to 100					
TFJ-2P	Fuel Injection	CFT2a	-425 to 100			x		•
TP PBS	Fuel Pump Balance Piston Sump	PFT4	-425 to -3	75 x			×	
TFPD-1P	Fuel Pump Discharge	PFT1	-425 to -39	90 x	×			

#### TABLE III-1 (Continued)

AEDC Code	Parameter	Tap No.	Range	Digital Data System	Magnetic Tape	Oscillo- graph	Strip Chart	Event X-Y Recorder Plotter
	Temperatures		<u>°</u>					
TFPD-2P	Fuel Pump Discharge	PFT1	-425 to 100	· ×		•		
TFPI-1	Fuel Pump Inlet	KFT2	-425 to -400	×				x
TFPI-2	Fuel Pump Inlet	KPT2a	-425 to 100	×				x
TFRT-1	Fuel Run Tank		-425 to -400	) x				
TFRT-3	Fuel Run Tank		-425 to -400	) x				
TFTC-1	Fuel Turbine Cone		-400 to 1800	х (				
TFTC-2	Fuel Turbine Cone		-400 to 1800	) x				
TFT 1-3	Fuel Turbine Inlet	TGT1	-300 to 2400	) x			x	
TFT 1-4	Fuel Turbine Inlet	GGT2 and GG2	-300 to 2000	x		×	×	
TFVC	Fuel Repressuriza- tion at Customer Connect Panel		-300 to -100	) x				
TPVL	Fuel Repressuriza- tion Nozzle Inlet	KHPT1	-300 to -100	×				
THET-1P	Helium Tank	NXTI	-200 to 150	×				(X
The VS-1	Main Fuel Valve Skin (Outer Wall)		-425 to 100	x			x	
THEVS-2	Main Fuel Valve Skin (Inner Wall)		-425 to 100	x			x	
TNODP .	Oxidizer Dome Purge at Customer Connect Panel		-250 to 200	x				
TOINL	Oxidizer Idle Mode Line	POT5	-300 to 100	x				
TOJ	Oxidizer Injection	COT1	-300 to 120	0 x		×		
TOPBC	Oxidizer Pump Beering Coolant	POT4	-300 to -25	0 x				
TOPD-1P	Oxidizer Pump Discharge	POT3	-300 to -25	0 x				
TOPD-2P	Oxidizer Pump Discharge	POT3	-300 to 100	×				
TOPI-1	Oxidizer Pump Inlet	KOT2	-310 to -25	0 x				x
TOPI-2	Oxidizer Pump Inlet	KOT2a	-310 to 100	×				×
TORT-1	Oxidizer Run Tank		-300 to -28	5 x				
TORT-3	Oxidizer Run Tank		-300 to -28	5 x				
TOTI-1P	Oxidizer Turbine Inlet	TGT3	0 to 120	0 x				
TOTH-1	Oxidizer Turbine Manifold		-300 to 100	0 x				
TOTH-2	Oxidizer Turbine Wanifold		-300 to 100	0 x				
TOTO-1P	Oxidizer Turbine Outlet	TGT4	0 to 100	0 x				
TOTSDL	Oxidizer Turbine Seal Drain Line		-100 to 100	0 x				
TOVC	Oxidizer Repressuriza- tion at Customer Connect Panel		-200 to 500	x				
TOVL	Oxidizer Repressuriza- tion Nozzle Inlet	KHOT1	-200 to 500	×				
TPIP-1P	Instrumentation Package		-300 to 200	×				

#### AEDC-TR-69-44

#### TABLE III-1 (Concluded)

AEDC Code	Parameter	Tap No.	Range	Digital Data System	Magnetic	Oscillo- graph		Event Z-Y Recorder Photon
	Temperatures		<u>.,</u>					
TPTU	Photocon Cooling Water (Upstream)		0 to 300	×				
TSCGA-1	Solid-Propellant Turbine Starter No. 1 Conditioning Ga	•	-100 to 200	x				
TSCGA-2	Solid-Propellant Turbin Starter No. 2 Conditi Gas		-100 to 200	x				
TSCGA-3	Solid-Propellant Turbine Starter No. 3 Conditioning Ga	•	-100 to 200	x				
TSCMF-1	Solid-Propellant Turbin Starter Case Mount Fl		0 to 1500	) x				
TSCMF-2	Solid-Propellant Turbin Starter Case Mount Fl		0 to 150	) x				
TSCMF-3	Solid-Propellant Turbiz Starter Case Hount Fl		0 to 150	× •				
TTCP	Thrust Chamber Purge		-250 to 200	×				
TTCT-E	Thrust Chamber Tube (Ex	it)	-425 to 500	×				
TTCT-T1	Thrust Chamber Tube (Ti	roat)	-425 to 500	×			×	
TTCT-T2	Thrust Chamber Tube (Ti	roat)	-425 to 500	x				
	<b>Vibrations</b>		g's					
UFPR	Fuel Pump	PZA-1	450 peak		×			
UFTR	Fuel Turbine	V123-2	450 peak		x			
UOPR	Oxidizer Pump	PZA-2	300 peak		×			
UTCD-1	Thrust Chamber Dome	FZA-la	1400 peak		×	×		
UTCD-2	Thrust Chamber Dome	FZA-2	1400 peak		×	×		
UTCD-3	Thrust Chamber Dome	PZA-3	300 peak		×	x		
	Voltage		volts					
VCB	Cootrol Bus		0 to 36	×				
VIB	Ignition Bue		0 to 36	×				
VIDA-1	Ignition Detect Amplif	ier	9 to 16	×				
VIDA-2	Ignition Detect Amplif	ier	9 to 16	I				
VPUVEP	Propellant Utilization Telemetry Potentione Excitation		0 to 5	x				

TABLE III-2
INSTRUMENTATION LIST FOR IDLE-MODE OPERATION

				Digital					
AEDC Code	Parameter	Tap No.	Range	Data System	Magnetic Tape	Oscillo- graph	Strip Chart	Event Recorder	X-Y Plotter
	Current		anp						
ICC	Control		0 to 30	x					
IIC	Ignition		0 to 30	×					
	Event		Counte						
EASIS-1	Augmented Spark Igniter No. 1 Spark		On/Off					x	
EASIS-2	Augmented Spark Igniter No. 2 Spark		On/Off					×	
EECL	Engine Cutoff Lockin		On/Off	×		×		×	
EECO	Engine Cutoff Signal		On/Off	×		x		x	
EER	Engine Ready Signal		On/Off					x	
EES	Engine Start Command	_	On/Off	×		x		<b>x</b> .	
KESCO	Programmed Duration Cutof		On/Off					' X	
EFBVO EFPCO	Fuel Bleed Valve Open Lim Fuel Pump Overspeed Cutof		On/Off On/Off					X	
EFPVC	Fuel Prevalve Closed Limi		On/Off	x				×	
EFPVO	Fuel Prevalve Open Limit	•	On/Off	×				×	
epua	Exploding Bridge Vire Firing Units Armed		On/Off	-				x	
EHCS	Helium Control Solenoid Energized		On/Off	x	x	* '		×	
EHGTC	Hot Gas Tapoff Valve Closed Limit		On/Off					x	
ehgto	Hot Gas Tapoff Valve Open Limit		On/Off					x	
EID	Ignition Detected		On/Off	x		x		x	
EIDA-1	Ignition Detect Amplifier No. 1		On/Off					x	
EIDA-2	Ignition Detect Amplifier No. 2		On/Off					**	1
EIMCS	Idle-Mode Control Solenoi Energized		On/Off	x		×		×	
EIMAC	Idle-Mode Valve Closed Li		On/Off					X	
ENCL	Idle-Mode Valve Open Limi Main-Stage Cutoff Lockin	t	On/Off On/Off					<b>x</b>	
ENCS	Main-Stage Control Soleno	id	On/011 On/011					x	
END-1	Energized No. 1 Main-Stage "OK"		On/Off					x	
	Depressurized .		-					-	
END-2	No. 2 Main-Stage "OK" Depressurized		On/Off		•			×	
ENFVC	Nain Fuel Valve Closed Limit		On/Off					<b>x</b>	
EMOAC EMEAQ	Main Fuel Valve Open Lini Main Oxidizer Valve Close		On/Off On/Off						
ENOVO	Limit Hain Oxidizer Valve Open		0n/011					×	
EMP-1	Limit No. 1 Main-Stage "OK"		On/Off					' x	
ENP-2	Pressurized No. 2 Main-Stage "OK"		On/Off					- x	
EMPCO	Pressurized Main-Stage Pressure Cuto	tt	On/Off					*	
-	Signal								
ens Ensco	Main-Stage Start Signal		On/Off On/Off					x	
ENSS	Duration Cutoff  Main-Stage Start Solenoic Energized	1	On/Off					×	
EOBAO	Oxidizer Bleed Valve Oper Limit	1	On/Off					×	
EOCO	Observer Cutoff Signal		On/Off					x	

TABLE III-2 (Continued)

				Digital				
AEDC	Davamatan	Tap	Proce	Data System		Oscillo-	Strip Event Chart Recorder	X~Y Plotter
Code	Parameter	No.	Raoge	O/Brow	Tape	graph	CHETT RECOIDES	Pioner
	Event							
EOPCO	Oxidizer Pump Overspeed Cutoff Signal		On/Of t				×	
EOPVC	Oxidizer Prevalve Closed Limit		On/Off	x			*	
EOPVO	Oxidizer Prevalve Open Limit	•	On/Off	×			x	
EOTCO	Fuel Turbine Over- Temperature Cutoff		On/Off				×	
eras is—1	Augmented Spark Igniter No. 1 Spark Rate		On/Off			×		
erasis=2	Augmented Spark Igniter No. 2 Spark Rate		On/Off			×		
ESAMCO	Stall Approach Monitor Cutoff		On/Off				×	
ESPTS	Solid-Propellant Turbine Starter Initiated	i	On/Off				x	
ESR-1	No. 1 Solid-Propellant Turbine Starter Ready		On/Off				×	
ESR-2	No. 2 Solid-Propellant Turbine Starter Ready		On/Off				x	
ESR-3	No. 3 Solid-Propellant Turbine Starter Ready		On/Off				<b>x</b>	
ESTCO .	Start "OK" Timer Cutoff		On/Off				x	
ETCBC	Thrust Chamber Bypass Valve Closed		On/Off				×	
ETCB0	Thrust Chamber Bypass Valve Open		On/Off				x	
EVSC-1	Vibration Safety Counts No. 1		On/Off			×		
EVSC-2	Vibration Safety Counts No. 2		On/Off			×		
EVSC-3	Vibration Safety Counts No. 3		On/Off			x		
	Flows		gpm					
QF-1	Engine Fuel Flow	PFF	0 to 11,000	x				
QF-2	Engine Fuel Flow	PFFR	0 to 11,000	×		×		
QF-3	Engine Fuel Flow	PFF	0 to 11,000			×		
QF-15AM	Fuel Flow Stall Approach Monitor			×		×		
QO-1	Engine Oxidizer Flow	POF	0 to 3600	×				
QO-2	Engine Oxidizer Flow	POFa	0 to 3600	×		×		
QO-3	Engine Oxidixer Flow	POF	0 to 3600			×		
*n	Forces		1b <sub>f</sub>					
	701000							
FSP-1 FSY-1	Side Load (Pitch)		±20,000	x x		x		
F81-1	Side Load (Yaw) Position		±20,000 Percent Open			^		
						_		
LFVT Limt	Main Fuel Valve		0 to 100 0 to 100	×		x x		
TIME	Idle-Node/Augmented Spa Ighiter Oxidizer Valv	e E	0 to 100	•		^		
LPUTOP	Propellant Utilization Valve		5 volts	x		×	x	
	Pressure		peia					
PA-1	Test Cell		0 to 0.5	×				
PA-2	Test Cell		0 to 1.0	×				
PA-3	Test Cell .		0 to 5.0	x		×		
PC-2PL	Thrust Chamber	CGla-1	0 to 50	x			x	
PPAS I J—L	Augmented Spark Igniter Fuel Injection	CF4	0 to 50	x				

TABLE III-2 (Continued)

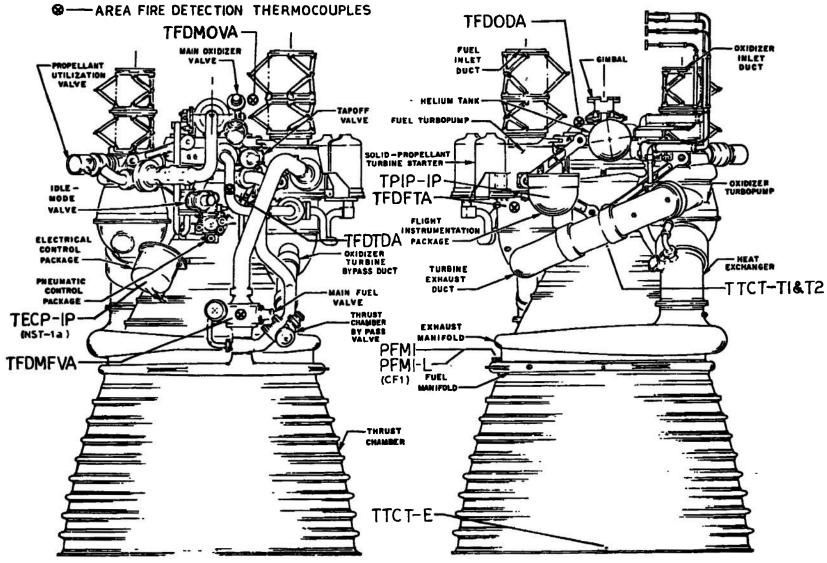
	netic Oscillo- Strip Event X-Y ape graph Chart Recorder Plotter
Pressure	
PFCO-L Film Coolant Orifice CF5 0 to 50 x	
PFJ-1L Fuel Injection CF2 0 to 50 x	
PFNI Fuel Jacket Manifold CF1 0 to 2000 x Inlet	
PFNI-L Fuel Jacket Manifold CF1 0 to 50 x Inlet	
PFPD-1L Fuel Pump Discharge PF3 0 to 50 x	
PFFI-1 Fuel Pump Inlet PF1 0 to 100 x	x x
PFPI-2 Fuel Pump Inlet 0 to 100 x	×
	x x
PFUT Fuel Ullage Tank 0 to 100 x	
PHEA Helium Accumulator NN3 0 to 750 x	
PHES Helium Supply 0 to 5000 x	
PHET-1P Helium Tank NN1-1 0 to 5000 x	x
PHET-2P Helium Tank NN1-3 0 to 5000 x	
PHRO-1P Helium Regulator NN2 0 to 750 x Outlet	
PNODP Oxidizer Dome Purge 0 to 750 x at Customer Connect Panel	
POASIJ-L Augmented Spark 103 0 to 50 x Igniter Oxidizer Injection	
POINL-L Oxidizer 1dle-Mode PO10 0 to 50 x Line	
POJ-2 Oxidizer Injectinn CO3s 0 to 2000 x	x
POPD-1L Oxidizer Pump Discharge PO3 0 to 50 x	
POPI-1 Oxidizer Pump Inlet PO1 0 to 100 x	×
POPI-2 Oxidizer Pump Inlet 0 to 100 x	x
	x x
POUT Oxidizer Ullage Tank 0 to 100 x	
PPTD Photocon Cooling Water 0 to 100 x (Downstream)	
PPTU Photocon Cooling Water 0 to 100 x (Upstream)	
PTCFJP Thrust Chamber Fuel 0 to 200 x Jacket Purge	
PTM-L Tapoff Manifold GG2b 0 to 50 x  Speeds rpm	
	_
NFP-2 Fusl Pump PPV 0 to 33,000	x
NFP-3 Fuel Pump PPV 0 to 33,000	<b>x</b>
NOP-2 Oxidizer Pump POV 0 to 12,000	x
NOP-3 Oxidizer Pump POV 0 to 12,000  Temperatures °F	x
TA-1 Test Cell North -50 to 800 x	
TA-2 Test Cell East -50 to 800 x	
TA-3 Test Cell South -50 to 800 x	
TA-4 Test Cell West -50 to 800 x	
TECP-1P Electrical Control NST1a -300 to 200 x	
TFASIJ Augmented Spark IFT1 -425 to 100 x Igniter Fuel Injection	ж
TFD-AVG Fire Detection Average 0 to 1000 x	x
TFDFTA Fire Detect Fuel Turbine 0 to 500 x Manifold Area	

#### TABLE III-2 (Continued)

AEDC Code	Parameter	Tap No.	Range	Digital Data Systen	Magnetic Tape	Oscillo- graph	Strip Chart	Event Recorder	X-Y Plotter
	Tenperatures								
TFDUFVA	Fire Detect Main Fuel Valve Area		0 to 500	×					
TFDMOVA	Fire Oetect Nain Oxidizer Valve Area		0 to 500	x					
TFDOOA	Fire Detect Oxidizer Dome Area		0 to 500	×					
TFDTDA	Fire Oetect Tapoff Duct Area		0 to 500	x					
TFJ-1P	Fuel Injection	CFT2	-425 to 100	×					
TFJ-2P	Fuel Injection	CFT2a	-425 to 100	x		x			
TFPBS	Puel Pump Balance Piston Sump	PFT4	-425 to -37	5 x			×		
TFPD-1P	Fuel Pump Discharge	PFT1	-425 to -39	0 x	×				
TFPD-2P	Fuel Pump Oischarge	PFT1	-425 to 100	x					
TFPI-1	Fuel Pump Inlet	KFT2	-425 to -40						x
TFPI-2	Fuel Pump Inlet	KFT2a	-425 to 100	×					×
TPRT-1	Fuel Run Tank		-425 to -40	0 x					
TFRT_3	Fuel Run Tank		-425 to -40	0 x					
TFTI-3	Fuel Turbine Inlet	TCT 1	-300 to 240				x		
TFT I—4	Fuel Turbine Inlet	GG2 and GGT2	-300 to 200	00 x		x	x	•	
THET-1P	Helium Tank	NNTI	-200 to 150	) x					×
TMFVS-1	Main Fuel Valve Skin (Outer Wall)		-425 to 100				×		
TMFVS-2	Main Fuel Valve Skin (Inner Wall)		-425 to 100	x			x		
TNODP	Oxidizer Dome Purge at Customer Connect Pan		-250 to 200	) x			•		
TOIML	Oxidizer Idle-Mode Lin	e POT5	-300 tn 100	) x					
LOT	Oxidizer Injection	COT1	-300 to 120	00 x		×			
TOPBC	Oxidizer Pump Bearing Coolant	POT4	-300 to −25	50 x					
TOPD-1P	Oxidizer Pump Discharg	e POT3	-300 to -25						
TOPD-2P	Oxidizer Pump Oischarg		-300 to 100						
TOPI-1	Oxidizer Pump Inlet	кот2	_310 to _2						x
TOPI-2	Oxidizer Pump Inlet	KOT2a	-310 to 100						x
TORT-1	Oxidizer Run Tank		-300 to -2						
TORT-3	Oxidizer Run Tank		-300 to -2						
TOTM-2 TOTSDL	Oxidizer Turbine Manif Oxidizer Turbine 5eal	old	-300 to 100						
	Drain Line	4.00	000 4- 00						
TPIP-1P TPTU	Instrumentation Packag		-300 to 200 0 to 300	0 x					
TTCP	(Upstream)		-250 to 20	0 x					
TTCT-E	Thrust Chamber Purge Thrust Chamber Tube (1		-425 to 50						
TTCT-T1	Thrust Chamber Tube (		-425 to 50				×		
TTCT-T2	Thrust Chamber Tube (7		-425 to 50						
	Vibrations		g's						
UFPR	Fuel Pump	PZA-1	450 Peak		×				
UFTR	Fuel Turbine	V123-2	450 Peak		×				
UOPR	Oxidizer Pump	PZA-2	300 Peak		×				
UTCD-1	Thrust Chamber Dome	FZA-la	1400 Peak		x	x			_
UTCD-2	Thrust Chamber Dome	FZA-2	1400 Peak		x	×			
UTCD-3	Thrust Chamber Dome	FZA-3	300 Penk		×	x			

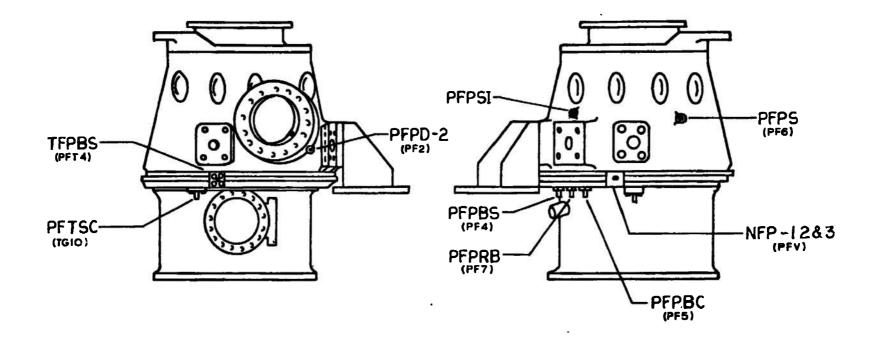
#### TABLE III-2 (Concluded)

APDC	Parameter	Tap No.	Range	Digital Data System	Magnetic Tape	Oscillo- graph	Strip	Event Recorder	X-Y Plotter
	<b>Voltage</b>		Volta						
VCB	Control Bus		0 to 36	x					
VIB	Ignition Bus		0 to 36	x					
VIDA-1	Ignition Detect Amplifier		9 to 16	×				-	
VIDA-2	Ignition Detect Amplifier		9 to 16	×					

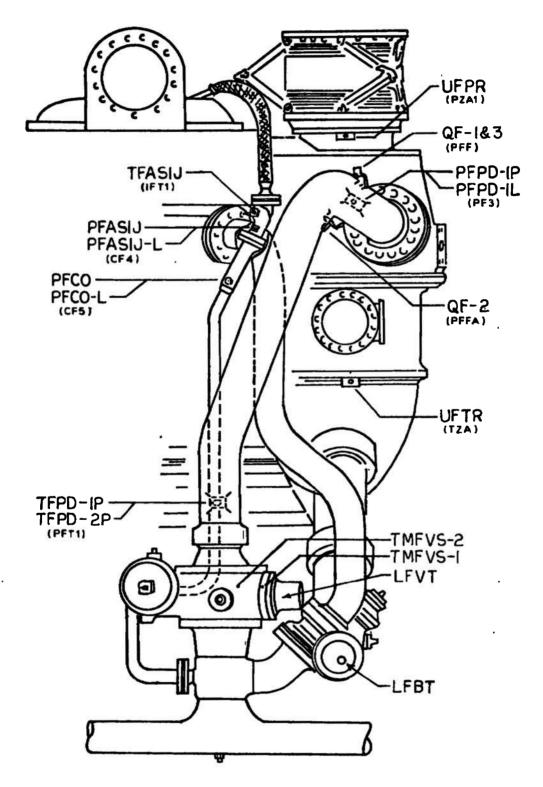


a. General Arrangement

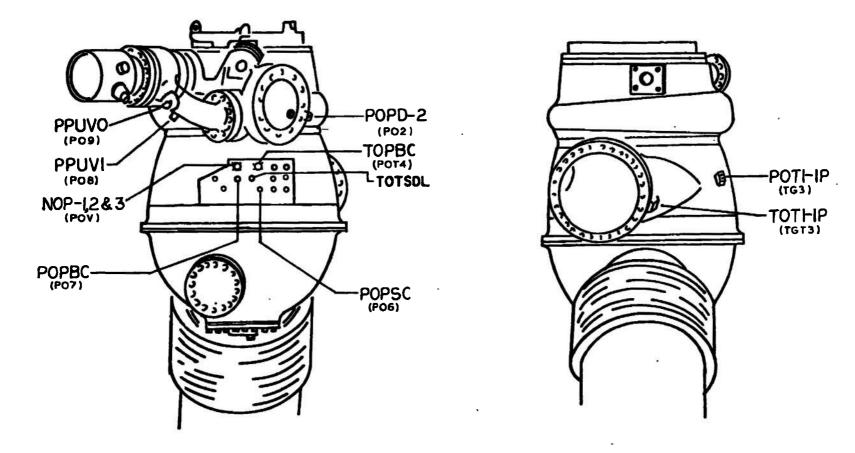
Fig. III-1 Selected Sensor Locations



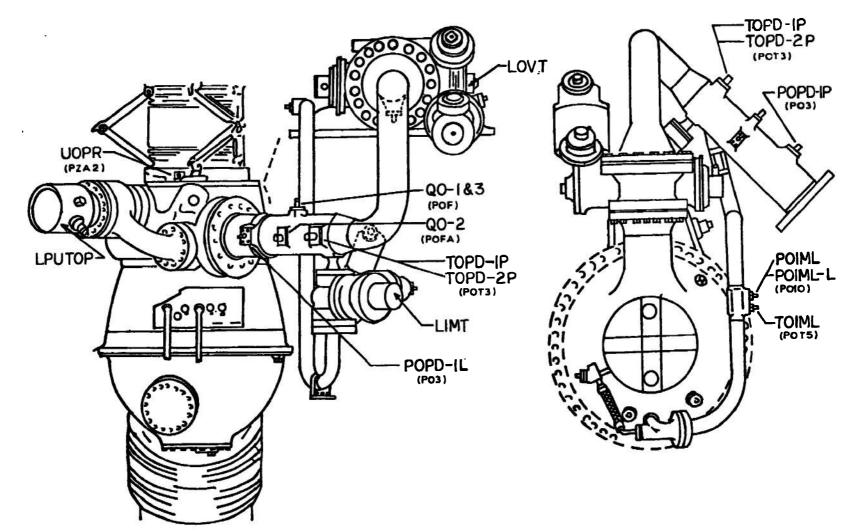
b. Fuel Turbopump Sensor Locations
Fig. III-1 Continued



c. Fuel System Sensor Locations
Fig. 111-1 Continued



d. Oxidizer Turbopump Sensor Locations
Fig. III-1 Continued



e. Oxidizer System Sensor Locations
Fig. III-1 Continued

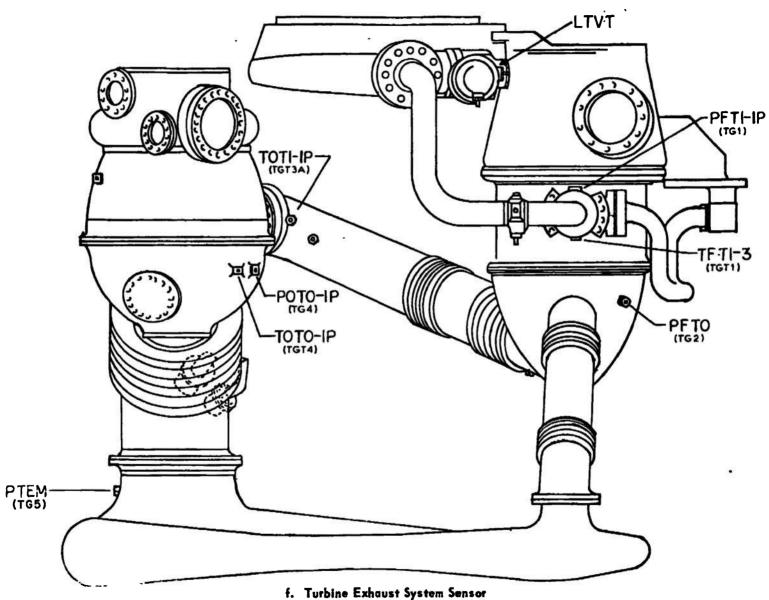
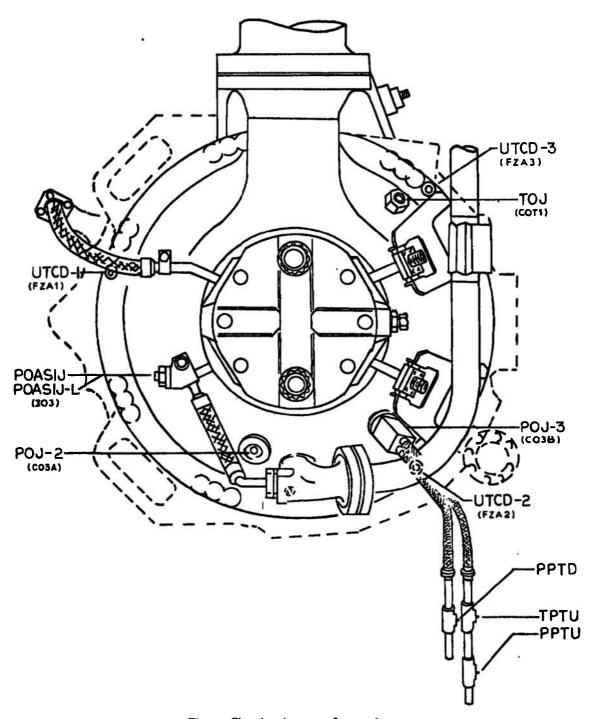
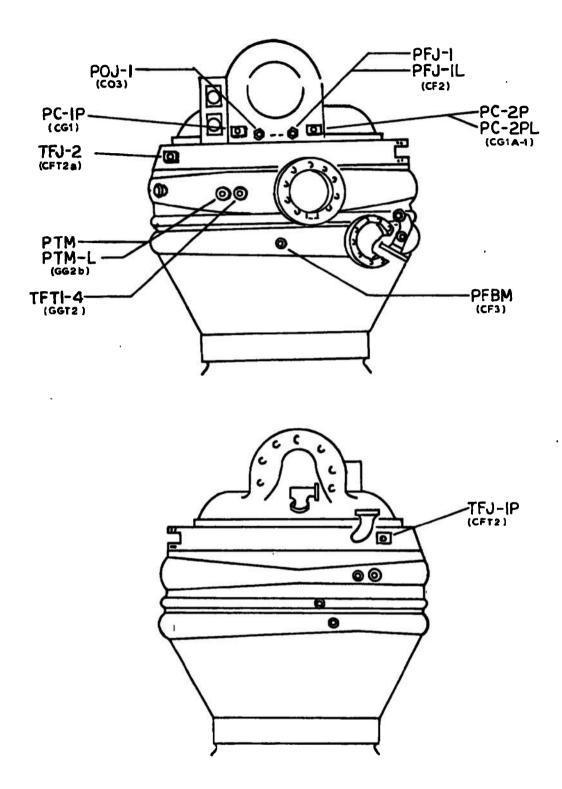


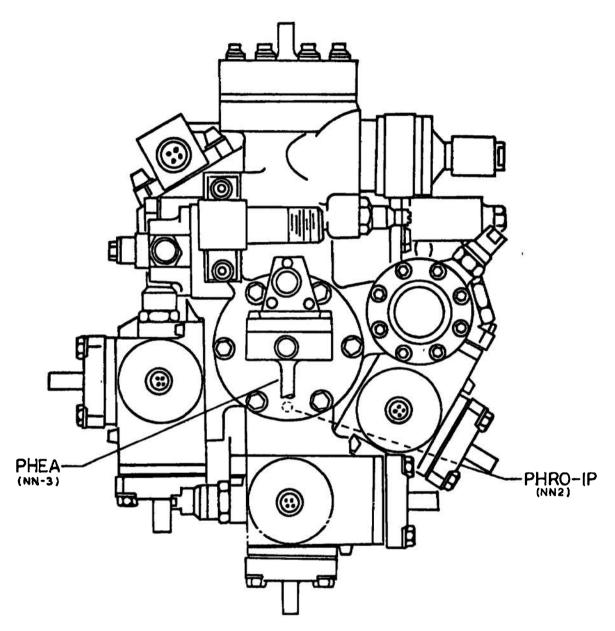
Fig. III-1 Continued



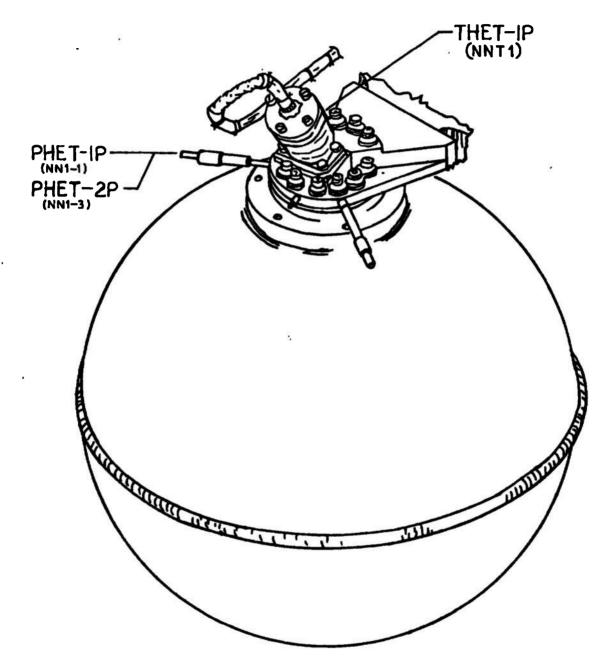
g. Thrust Chamber Injector Sensor Locations
Fig. III-1 Continued



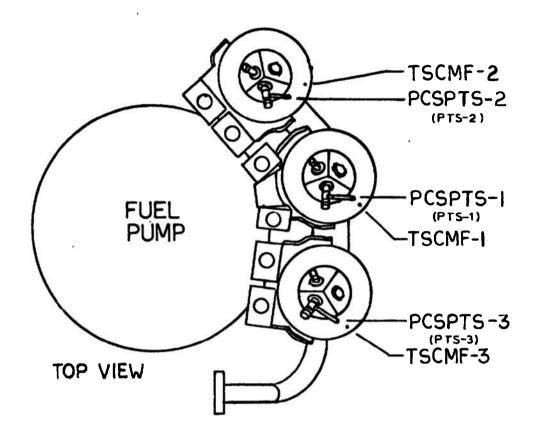
h. Thrust Chamber Sensor Locations Fig. III-1 Continued

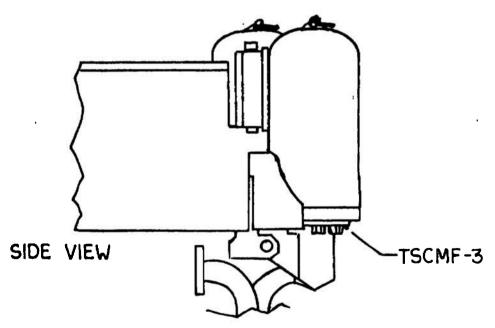


i. Pneumatic Control Package Sensor Locations Fig. III-1 Continued

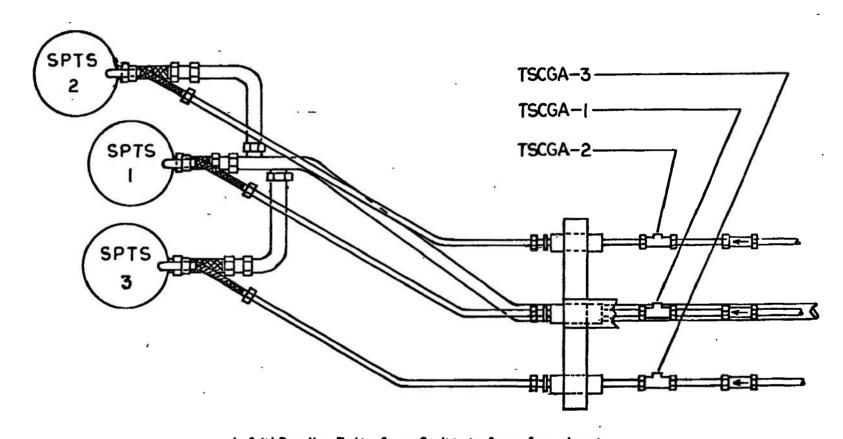


j. Helium Tonk Sensor Locations Fig. III-1 Continued

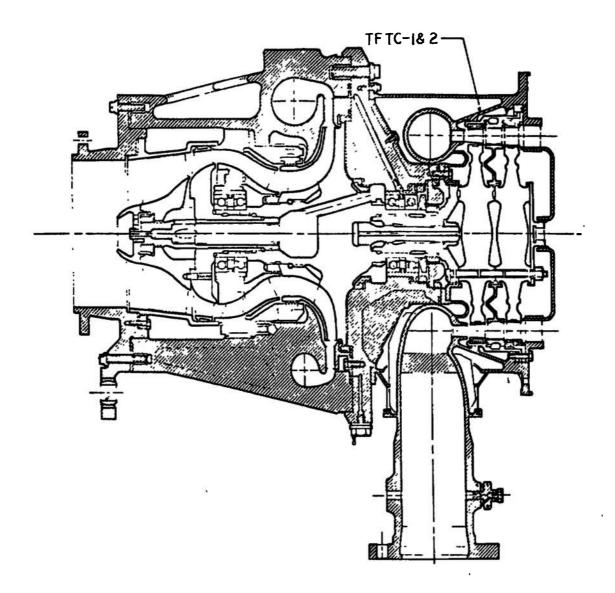




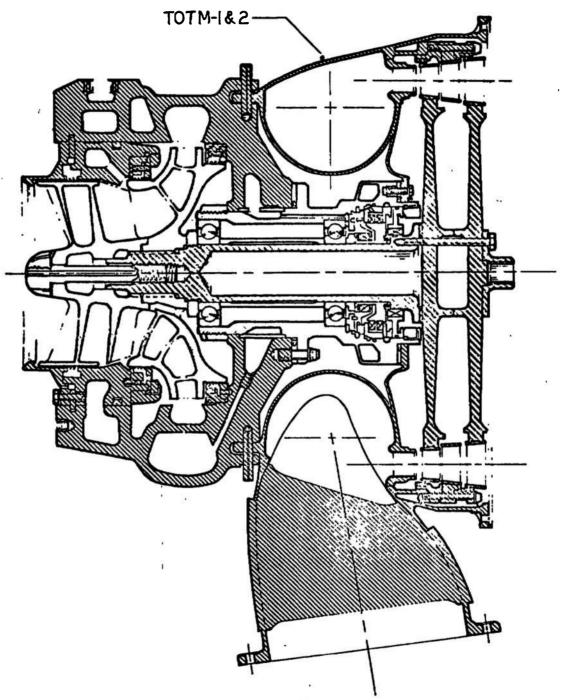
k. Solid-Propellant Turbine Starter Sensar Locations
Fig. III-1 Continued



1. Solid-Propollant Turbine Starter Conditioning System Sensor Locations
Fig. III-1 Continued

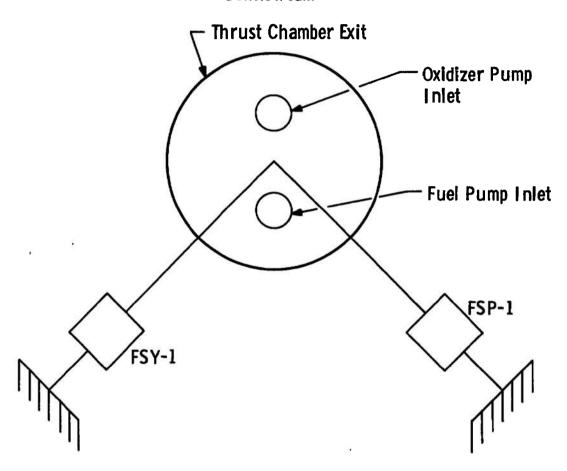


m. Fuel Turbine Sensor Locations
Fig. III-1 Continued

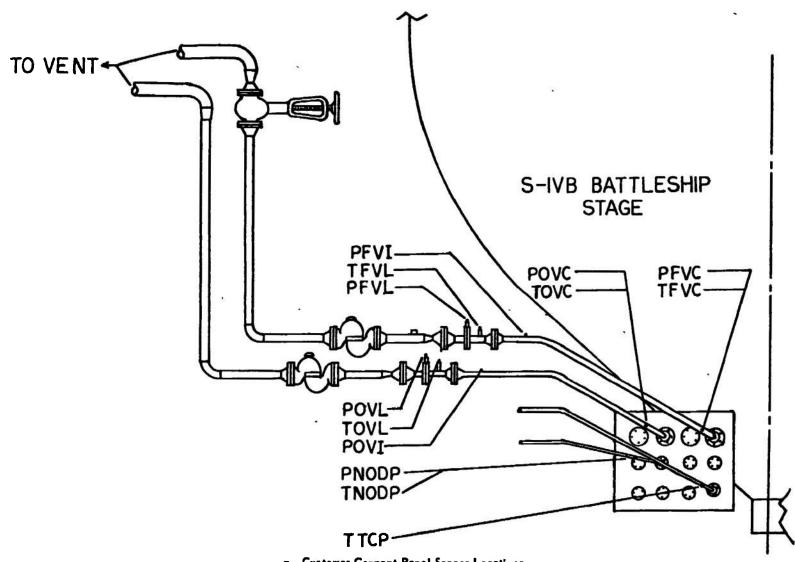


n. Oxidizer Turbine Sensor Locations Fig. III-1 Continued

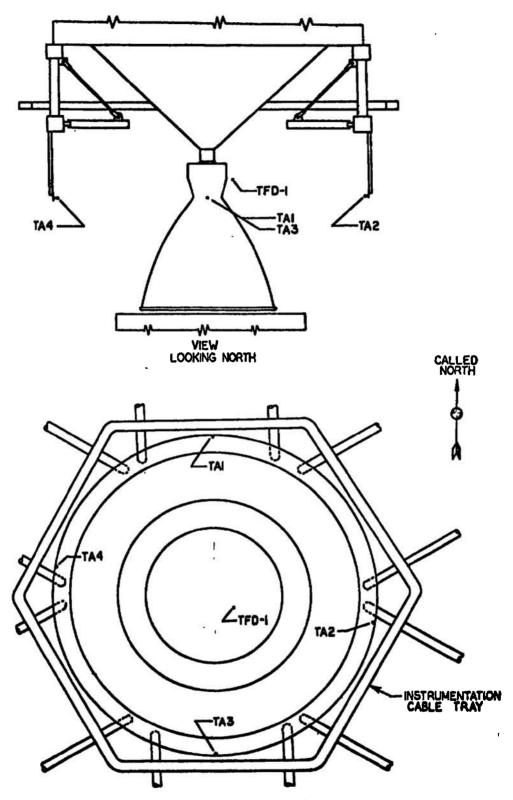
### View Looking Downstream



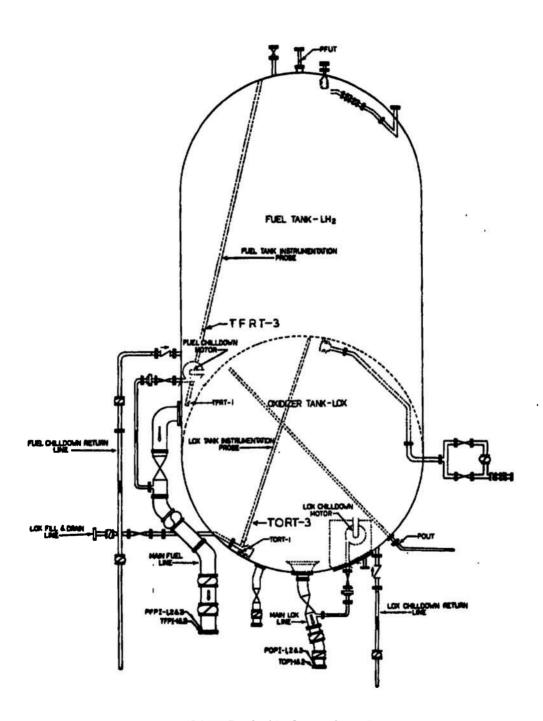
o. Side Load Forces Sensor Locations Fig. III-1 Continued



p. Customer Connect Panel Sensor Locations
Fig. 111-1 Continued



q. Test Cell Ambient Temperature Sensor Locations
Fig. 111-1 Continued



r. S-IVB Battleship Sensor Locations Fig. III-1 Concluded

Security Classification

#### DOCUMENT CONTROL DATA - R & D (Security classification of title, body, of abstract and indexing ennotation must be entered when the overall report is classified) 1. ORIGINATING ACTIVITY (Corporate author) 2a. REPORT SECURITY CLASSIFICATION Arnold Engineering Devélopment Center UNCLASSIFIED ARO, Inc., Operating Contractor Arnold Air Force Station, Tennessee 2b. GROUP N/A ALTITUDE DEVELOPMENTAL TESTING OF THE J-2S ROCKET ENGINE IN PROPULSION ENGINE TEST CELL (J-4) (TESTS J4-1902-01 THROUGH J4-1902-04) 4. DESCRIPTIVE NOTES (Type of report and inclusive dates) December 5, 1968 through January 10, 1969 - Interim Report 5. AUTHOR(S) (First name, middle initial, last name) N. R. Vetter, ARO, Inc. 74. TOTAL NO. OF PAGES 6. REPORT DATE 7b. NO. OF REFS February 1969 113 60. CONTRACT OR GRANT NO. F40600-69-C-0001 9a, ORIGINATOR'S REPORT NUMBER(5) AEDC-TR-69-44 b. PROJECT NO. 9194 9b. OTHER REPORT NO(\$) (Any other numbers that may be assigned this report) .System 921E N/A 10. DISTRIBUTION TATEMENT Each transmittal of this document outside the Department of Defense must have prior approval of NASA, Marshall Space Flight Center (I-E-J), Huntsville, Alabama 35812. 11. SUPPLEMENTARY NOTES 12. SPONSORING MILITARY ACTIVITY NASA, Marshall Space Flight Available in DDC. Center (I-E-J) Huntsville, Alabama 35812

Five firings of the Rocketdyne J-2S rocket engine (S/N J-111A) were conducted in Test Cell J-4 of the Large Rocket Facility between December 5, 1968, and January 10, 1969. These firings were accomplished during test periods J4-1902-01 through J4-1902-04 at pressure altitudes of approximately 100,000 ft at engine start to investigate engine idle-mode operation, transition from idle mode to main stage, and steady-state operation at main stage. The engine started successfully in all cases and two planned transitions from idle mode to main stage were accomplished. The thrust chamber and injector were damaged extensively during a 288.5-sec duration idle-mode firing (04A).

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18. ABSTRACT

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14. KEY WORDS	LINI	LINK B		LIN	кс	
	ROLE	WT	ROLE	WT	ROLE	WT
J-2S rocket engines Saturn liquid propellants altitude simulation flight simulation startup performance tests performance evaluation damage	5		eri C			

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